



# Particle-based modelling of axisymmetric tandem mirror devices

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In this work, we describe the use of a 1D-2V quasi-neutral hybrid electrostatic PIC with Monte-Carlo Coulomb collisions and non-uniform magnetic field to model the parallel transport and confinement in an axisymmetric tandem mirror device. End-plugs, based on simple-mirrors, are positioned at each end of the device and fueled with neutral beams (25 and 100 keV) to produce a sloshing ion population and increase the density of the end-plugs relative to the central cell. Results show the formation of a potential difference barrier between the central cell and the end-plugs. This potential confines a large fraction of the low energy thermal ions in the central cell which would otherwise be lost in a simple mirror, demonstrating the advantage of the beam-driven tandem mirror configuration relative to simple mirrors. In addition, we explore the effect of end-plug electron temperature on the confinement time of the device and compare it with theoretical estimates. Finally, we discuss the limitations of the code in its present form and describe the next logical steps to improve its predictive capability such as a fully nonlinear Fokker–Planck collision operator, multiply nested flux surface solutions and modeling the exhaust region up to the wall.

**Key words:** Fusion Plasma, Plasma Confinement, Plasma Simulation

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## 1. Introduction

With High-Temperature Superconducting (HTS) magnet technology becoming available, several private companies are pursuing their use to develop break-even type fusion devices. The use of HTS allows the operation at magnetic field strengths not otherwise practical. This capability opens parameter space previously unexplored which offers optimizations such as drastic reduction in plasma volumes required to reach break-even conditions (Whyte 2019). Both tokamak and mirror-based devices

are currently under consideration (Whyte *et al.* 2016; Endrizzi *et al.* 2023; Forest *et al.* 2018).

Although both tokamak and mirror-based concepts rely on magnetic confinement of high temperature plasmas, Radio-Frequency (RF) heating and Neutral Beam Injection (NBI) for plasma heating and fueling, there are important physics differences between the two concepts that require special attention and new numerical codes to enable predictive modeling and design of new devices. In the case of mirror devices, one key characteristic is the presence of anisotropic (non-Maxwellian) distribution functions to ensure plasma equilibrium. The non-Maxwellian nature of the plasma means that many of the approximations used in numerical modeling of toroidally-confined plasmas cannot be directly used and require adaptation to deal with the physics encountered in mirror-confined plasmas.

At CompX, several modeling efforts have been undertaken to advance the magnetic mirror concept. For example, the continuum Bounce-Average (BA) Fokker–Planck (FP) code CQL3D commonly used in tokamaks has been adapted to mirror geometry (CQL3D-m) and applied to model the Wisconsin High-field Axisymmetric Mirror (WHAM) (Endrizzi *et al.* 2023; Egedal *et al.* 2022) funded by the ARPA-E BETHE program and the Break-Even Axisymmetric Mirror (BEAM) device, in development by the private company Realta Fusion. Results from such efforts have been published in Endrizzi *et al.* (2023) and the latest results are under preparation for upcoming papers. These efforts relied entirely on the BA description of confined plasmas in simple mirrors. In order to extend treatment to multiple-mirror arrangements such as those encountered in tandem mirrors, the quasi-neutral hybrid Particle-In-Cell (PIC) code PICOS++, previously used to model the upcoming divertor simulator MPEX (Kumar *et al.* 2023), has been adapted to model axisymmetric tandem mirrors to understand the effect of end-plugs on the confinement of a central cell plasma. The main goal of this paper is to describe the current state of PICOS++, present results from its application to tandem mirror geometries, and discuss the next steps to improve predictive capability.

## 2. PICOS++

PICOS++ is an MPI-based parallel quasi-neutral 1D-2V hybrid electrostatic particle-in-cell (PIC) code which solves for the time-dependent ion distribution function along the dimension parallel to the magnetic flux while describing electrons as a fluid. At the present stage of development, the distribution function is solved only along a single finite-width flux surface. Its current use does not address Magneto-Hydrodynamic (MHD) or kinetic instabilities. Its primary use is directed towards calculating the evolution of the 1D-2V ion distribution function subject to various effects. The term ‘quasi-neutral’ refers to the assumption that the electron density is always given by the quasi-neutrality condition  $n_e = \sum n_\beta Z_\beta$ . This approximation means that its use precludes the sheath region where quasi-neutrality does not hold. The term ‘hybrid’ refers to use of kinetic ions and fluid electrons. In PICOS++, the electron energy equation is not solved, thus the electron profile is given as an input. In addition, PICOS++ computes the self-consistent electrostatic field parallel to the magnetic flux using Ohm’s law as a function of time and can handle Radio-Frequency (RF) heating, Neutral Beam Injection (NBI) and Coulomb collisions. PICOS++ has been successfully used to model the MPEX linear divertor simulator with fundamental ICRF heating (Kumar *et al.* 2023). An in-depth description of

PICOS++ and the associated framework has been presented in Kumar *et al.* (2023). In the present paper, we give a brief overview of the code.

### 2.1. Ion distribution function

The ion distribution function is expressed as in (2.1), where  $x$  is the coordinate along the magnetic flux and  $v_{\parallel}$  and  $v_{\perp}$  are the coordinates in velocity space parallel and perpendicular to the magnetic flux respectively. Each ion is assumed to have a random gyro-phase, and a zero-orbit width. Under these circumstances it is appropriate to use the term ‘drift kinetic ions’.  $A_0$  is a reference cross-sectional area associated with the finite-width of the flux surface. The ion distribution function is described with  $N_C$  computational particles or markers and each marker has a weight  $a_i$ . In phase space, each ion is described with a so-called shape function  $S$  to broaden its footprint and reduce shot noise that would arise with the use of delta functions. Shape function satisfy the expression in (2.2). The term  $K$  in (2.1) is the normalization constant which ensures that  $\int f d^3x d^3v = N_R$  where  $N_R$  is the total number of real particles contained in the volume enclosed by the flux surface of finite but small width.  $N_{SP}$  in (2.3) represents the sum of all the weights.

In PICOS++, ions are described as Guiding-Centers (GC) bound to the magnetic flux and the magnetic field is described in the paraxial limit (2.4). Conservation of the magnetic moment is used. The equations of motion for the ions, described in detail in Kumar *et al.* (2023), are time-integrated using a 4<sup>th</sup> order RK scheme. The time-step  $\Delta t_{RK}$  used in advancing particles is chosen such that on average, particles do not travel a distance greater than  $\Delta x$ , where  $\Delta x$  is the cell width length along the magnetic flux.

When markers leave/exit the computational domain, they are reintroduced into the simulation and their weight  $a_i$ , velocity  $\vec{v}_i$  and position  $x_i$  are selected to achieve a desired particle source in phase space or certain boundary conditions (reflecting or periodic). This allows the modelling of NBI or warm-plasma sources.

$$f(x, v_{\parallel}, v_{\perp}) = \frac{K}{A_0} \frac{B(x)}{B_0} \sum_i^{N_C} a_i S(x - x_i) S(v_{\parallel} - v_{\parallel i}) \frac{S(v_{\perp} - v_{\perp i})}{v_{\perp}} \quad (2.1)$$

$$\int_{-\infty}^{+\infty} S(x' - x_i) dx' = 1 \quad (2.2)$$

$$K = \frac{N_R}{N_{SP}} \quad N_{SP} = \sum_i^{N_C} a_i \quad (2.3)$$

$$B_r(r, x) = \frac{-r}{2} \frac{dB_x}{dx} \quad (2.4)$$

### 2.2. Parallel electric field

PICOS++ solves the electric field parallel to the magnetic flux at the cell centers of the mesh  $x_m$  using the electrostatic approximation  $E_{\parallel} = -\partial V / \partial x$  where  $V$  is the electric potential along the magnetic flux. In the quasi-neutral approach used in PICOS++, the parallel electric field is solved in the bulk plasma region using the Generalized Ohm’s law, (2.5), below. The electric field in the sheath (at the plasma-wall boundaries) is not resolved in this approximation; however, its effect

can be incorporated in the quasi-neutral model by adjusting the potential in the cell adjacent to the wall such that the total ion flux to the wall is equal to the thermal flux of electrons given their temperature. At present, PICOS++ does not have a sheath boundary condition. We note, however, that the electric field calculated by PICOS++ at the mirror throats does accelerate ions to conditions close to the ion sound speed. Application of the full sheath boundary condition will be the subject of future work. This will be especially important in modeling of the full exhaust-wall region.

The parallel electric field based on Ohm's law is given below in (2.5), where the electron density is given by quasi-neutrality  $n_e = \sum n_\beta Z_\beta$ , and the terms  $P_{e\parallel}$  and  $P_{e\perp}$  represent the parallel and perpendicular electron pressure. If the electron distribution function is taken to be Maxwellian and isotropic, we can further simplify the expression for the parallel electric field as in (2.6). Finally, if the electron temperature is taken to be uniform, this expression reduces to the classic Boltzmann relation between the electron density and electric potential.

In the present work, the electric field solution is obtained after every 200 particle advance time steps ( $\Delta t_{RK}$ ) as the evolution of the ion density and associated moments evolve over time scales much longer than the transit times of the ions over a cell. This procedure of separating the particle advance time steps from the calculation of ion moments and the parallel electric field significantly reduces computational time as more time is spent in parallel MPI execution while minimizing MPI communication time and overhead. Moreover, this process eliminates higher frequency fluctuating fields. Using this procedure, it becomes computationally practical to simulate thermalization of NBI in mirrors.

$$E_{\parallel} = \frac{-1}{en_e} \left( \frac{dP_{e\parallel}}{dx} - \left( \frac{P_{e\parallel} - P_{e\perp}}{B} \right) \frac{dB_x}{dx} \right) \quad (2.5)$$

$$E_{\parallel} = \frac{-1}{en_e} \frac{d}{dx} (n_e T_e) \quad (2.6)$$

### 2.3. Coulomb collisions

PICOS++ includes Coulomb collisions via a *linearized* Monte-Carlo Fokker-Planck collision operator as described in greater detail in reference (Boozer and Kuo-Petravic 1998; Caneses *et al.* 2020; Kumar *et al.* 2023). The operator is applied in the plasma frame of reference (traveling along the magnetic flux at the mean plasma speed) prior to the electric field calculation and scatters both the kinetic energy and pitch angle of each particle. The collision operator requires the moments of the ion distribution function at the current time step for all species (densities, parallel particle flux, temperatures) to evaluate the scattering rates. The change in kinetic energy  $E$  and cosine of pitch angle  $\xi$  of the  $i^{th}$  particle colliding with the  $j^{th}$  species in a time  $\Delta t$  are given in (2.7) and (2.8), where  $v_{ij}^E$  and  $v_{ij}^D$  are the energy loss and deflection rates. Their expressions are presented in reference (Kumar *et al.* 2023; Boozer and Kuo-Petravic 1998). A comparison between these operators and analytical solutions are presented in Appendix A.

$$\Delta E_{ij} = -2v_{ij}^E \Delta t \left[ E_{ij} - \left( \frac{3}{2} + \frac{E_{ij}}{v_{ij}^E} \frac{dv_{ij}^E}{dE} \right) T_j \right] \pm 2\sqrt{T_j E_{ij} v_{ij}^E} \Delta t \quad (2.7)$$

$$\Delta\xi_{ij} = -\xi_{ij}v_{ij}^D \pm \sqrt{(1 - \xi_{ij}^2)} v_{ij}^D \Delta t \quad (2.8)$$

An important limitation of the linearized collision operator in PICOS++ is that it neglects the velocity-space features of the ion distribution function by assuming that they are essentially drifting Maxwellians. Moreover, it does not conserve energy nor momentum. This approximation works well in cases where the distribution function does not deviate too far from drifting Maxwellian as in the case of linear divertor simulators where the plasma temperature is low enough to render the plasma very collisional and RF heating mainly extends the tail of the Maxwellian distributions (Kumar *et al.* 2023; Caneses *et al.* 2020); however, in the case of NBI and RF heated mirrors, this is no longer true as the distribution function is necessarily non-thermal in order to establish parallel force balance, and a Monte-Carlo fully non-linear Fokker-Planck collision operator (Wang *et al.* 1995; Takizuka and Abe 1977) is a requirement. We will discuss this topic further after the presentation of the results.

### 3. Results

In this section, we present numerical results for a tandem mirror configuration driven by a deuterium warm plasma source in the central cell, and two deuterium NB injectors each into the end-plugs. Two cases are presented, a 25 keV and a 100 keV deuterium beam case.

#### 3.1. Simulation setup

The magnetic field profile used in these simulations is presented in [figure 1](#) with the red trace (scale at right-hand side). The magnetic field at the central cell is about 0.85 T and the peak value of 8 T occurs at the mirror throats, giving a mirror ratio of about 9. A warm plasma source of  $1 \times 10^{20}$  deuterium ions per second at 1 keV is applied in the central cell. Two end-plug mirrors are located on either end of the central cell and each is fueled with either a 25 keV or 100 keV beam at 0.4 MW each. The end of the domain is taken to be at the throats of the outermost magnetic mirrors. At present, the exhaust region is currently not solved for. This will be the subject of future work. The electron temperature is described with a uniform profile at a value of 1 keV. Simulation parameters are presented in [table 1](#).

#### 3.2. 25 keV beam case

The simulation is started with a uniform electron density of  $5 \times 10^{18} \text{ m}^{-3}$ . Neutral beams are injected into the end-plugs at 45 degrees relative to the magnetic field at energy 25 keV from the start of the simulation. This case is evolved up to 22 ms. The electron density profile at various time steps is presented in [figure 1](#). Temporal evolution of the electron density in the end-plugs ( $x = 5 \text{ m}$ ) and the central cell is presented in [figure 2](#) showing beam thermalization, whereas the central cell density ( $x = 0 \text{ m}$ ) is still evolving.

The increase in density in the end-plugs is caused by accumulation of a sloshing ion population driven by the 45-degree neutral beams. At early times (5 ms), the formation of sloshing ion density peaks at the turning points can be clearly observed in [figure 1](#). As density and time increases, the sloshing ion population accumulates pitch angle scattering, begins to thermalize, and eventually form a single density

Simulation parameter	Physical value
Length of domain $L$	12 m
Left (right) boundary	−6 (+6) m
Number of spatial cells	264
Cell width	4.5 cm
Total simulation time	19 – 23 ms
Peak magnetic field $B^{\text{max}}$	8 T
Central cell magnetic field	0.85 T
Central cell plasma radius	0.05 m
Electron temperature	Uniform at 1 keV
Number of ion species	1
Ion species 1 mass number	2 AMU
Ion species 1, charge number	+ 1
Ion species 1, source 1	1e20 D+/sec warm plasma source at a temperature of 1 keV centered at 0 m, 0.5 m spread
Ion species 1, source 2 and 3	0.8 MW (total) 45-deg NBI source, centered at $\pm 5$ m, 0.1 m spread. Beam energy at 25 keV or 100 keV
Number of computational particles	$1 \times 10^6$
Particle advancing MPIs	20
Particle advance time step $\Delta t_{RK}$	$0.16 \mu s$
Electric field update time step	$2 \times 10^2 \Delta t_{RK}$

TABLE 1. Simulation parameters used in PICOS++ for tandem mirror simulations.

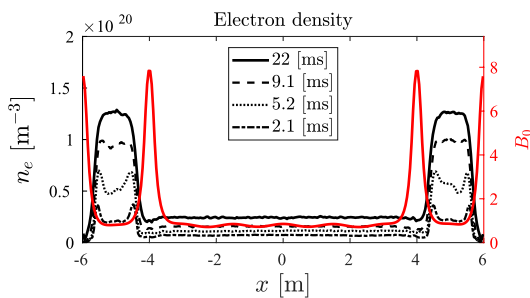


FIGURE 1. Electron density (black) along the length of the device for various simulation times (see legend). The magnetic field strength along the length of the computational domain is represented by the red trace. The NBI energy in each end-plug is 25 keV at 0.4 MW.

peak in the end-plug regions, saturating at a value of  $1.2 \times 10^{20} \text{m}^{-3}$  in about 15 ms. Beyond that time, the source of fast ions equals the scattering of fast ions out of the end-plugs.

The time-dependent ion temperatures (parallel and perpendicular) in the end-plugs are presented in figure 3. Perpendicular temperature is taken at the sloshing ion turning point while the parallel temperature is taken at the center of the end-plug where the parallel energy of the sloshing ions is maximum. At the very early stages of the simulation when the density is low, both the parallel and perpendicular temperature quickly increase to values close to the injection energy of the beams. As

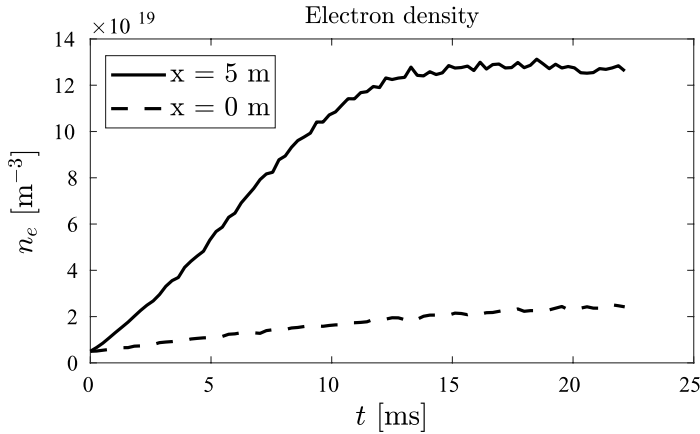


FIGURE 2. Electron density temporal evolution in the central cell (dashed) and end-plug (solid) region. The NBI energy in each end-plug is 25 keV at 0.4 MW.

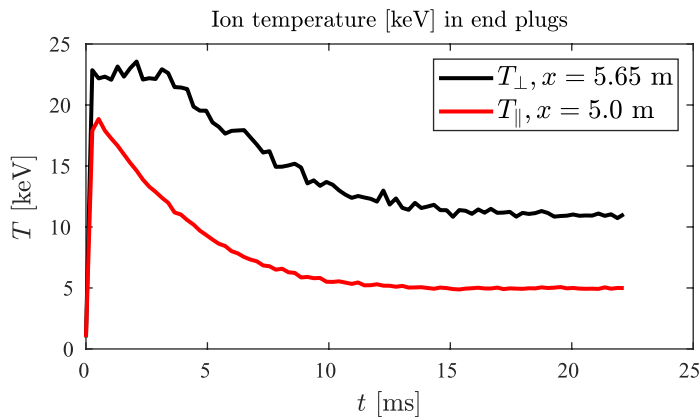


FIGURE 3. Parallel (red) and perpendicular (black) ion temperatures in the end-plugs. The perpendicular and parallel temperature is taken at the turning point of the sloshing ions density and mid plane of end-plugs respectively. The NBI energy in each end-plug is 25 keV at 0.4 MW.

time progresses, density accumulation increases the collisionality of the beams and eventually thermalization at a lower temperature is reached at around 15 ms.

It is worth noting from [figure 2](#) that the density in the central cell increases linearly throughout the entire simulation. As the density in the end-plugs increase, the confinement of the central cell plasma improves due to the formation of the electrostatic confinement potential  $\Delta V = V_{ep} - V_{cc}$  where the subscripts ‘ep’ and ‘cc’ refer to end-plugs and central cell respectively. The electric potential associated with the plasma density profile at 22 ms is presented in [figure 4](#) below. The potential difference between the central cell and the end-plugs  $\Delta V$  is approximately  $1.7T_e$  or 1.7 kV. For a central cell ion temperature of about 1 keV, this electrostatic potential can confine a large fraction of the warm plasma in the central cell. This will be



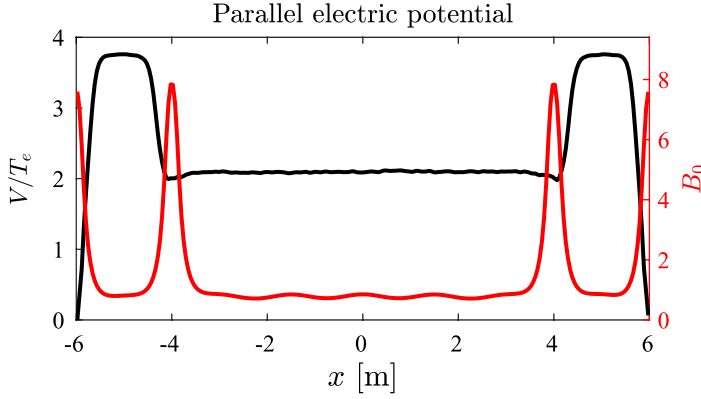


FIGURE 4. Parallel electric potential (black) and magnetic field strength (red) along the length of the device. The electron temperature is taken to be uniform at a value of 1 keV. The NBI energy in each end-plug is 25 keV at 0.4 MW.

shown more clearly with the presentation of the ion distribution function later in the paper.

Let us now consider the ion confinement time in the central cell given the conditions observed in the simulation (potential difference, plasma density, ion temperature). To carry this out, we use equations (2.2) and (2.3) from reference (Rognlien and Cutler 1980) for the confinement time  $\tau_i$  for a singly-charged ion in a square electrostatic well. These equations are presented in (3.1) and (3.2), where  $\tau_{ii}$  is the ion-ion scattering time,  $R$  the mirror ratio and  $T_{ic}$  the ion temperature in the central cell. Letting  $T_{ic} = 1$  keV,  $n = 3 - 4 \times 10^{19} \text{ m}^{-3}$  and  $m_i = 2m_p$ , we get an ion-ion scattering time  $\tau_{ii}$  of about 1–1.4 ms. Given the mirror ratio ( $R = 9$ ) and the potential difference ( $\Delta V = 1.7$  keV), the Pastukhov confinement time  $\tau_i$  falls between 21 and 29 ms.

$$\tau_i = \tau_{ii} \frac{\sqrt{\pi}}{2} \left( \frac{R+1}{R} \right) \ln(2R+2) \left( \frac{\Delta V}{T_{ic}} \right) \frac{\exp\left(\frac{\Delta V}{T_{ic}}\right)}{1 + \left(\frac{T_{ic}}{2\Delta V}\right)} \quad (3.1)$$

$$\tau_{ii} = \frac{4\pi\epsilon_0^2 m_i^2 v_i^3}{ne^4 \ln} \text{ where } v_i = \sqrt{2T_i/m_i} \quad (3.2)$$

We now compare the above Pastukhov confinement time estimates (21 and 29 ms) with the results from the simulation. To do this, we calculate the temporal evolution of the plasma density in the central cell and select the confinement time that best fits the results from PICOS++. The expression that describes this process is given in (3.3) (Kumar *et al.* 2023), where the mean plasma density in the central cell is represented by  $n$ , the particle generation rate by  $G$ , the central cell length by  $L$ , the mean cross sectional area of the central cell  $A$  and the confinement time by  $\tau_i$ . In this formulation we have used the approximation that the plasma density is practically uniform in the central cell as shown in figure 1. For a constant particle generation rate  $G$ , the solution to (3.3) is given in (3.4). The steady state solution ( $t \rightarrow \infty$ ) is given in (3.5).



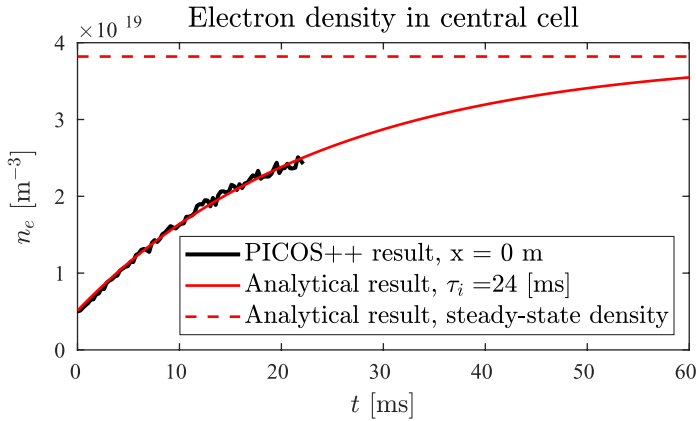


FIGURE 5. Temporal evolution of the central cell density calculated by PICOS++ (black) and analytical solution (red) using a confinement time of 24 ms. The red-dotted line represents the steady state value that is expected given the confinement time and particle generation rate.

Using a constant particle generation rate of  $1 \times 10^{20}$  particles per second (table 1), the temporal evolution of the plasma density in the central cell is compared with the results from PICOS++ in figure 5. The black trace represents the numerical data produced with PICOS++. The red trace is calculated using (3.3) with a confinement time of 24 ms which leads to the best fit to the numerical results. The horizontal red broken trace represents the steady state plasma density using (3.5). This comparison shows that the confinement time required to fit (3.3) to the numerical result ( $\tau_i = 24$  ms) is consistent to the confinement time calculated using the Pastukhov expression ( $\tau_i = 21$  to 29 ms) (3.1).

$$\dot{n} + \frac{n}{\tau_i} = \frac{G}{LA} \quad (3.3)$$

$$n(t) = n_0 \exp\left(-\frac{t}{\tau_i}\right) + \frac{G\tau_i}{LA} \left(1 - \exp\left(-\frac{t}{\tau_i}\right)\right) \quad (3.4)$$

$$n_{ss} = n_0 + \frac{G\tau_i}{LA} \quad (3.5)$$

At the edges of the computational domain, the potential drop between the center of the end-plug and the throat at the edge of the domain is close to  $3.8T_e$ . This potential drop accelerates ions towards the edge of the domain as shown in figure 6 to speeds approaching the ion sound speed given by  $c_s = \sqrt{e(T_e + T_i)/m_i}$ . To model the complete effect of the sheath, the potential drop at the wall needs to be set to make the ion flux equal to the electron flux retarded by the potential drop in the bulk plasma and sheath region. At present this sheath potential drop is not modeled; however, it is important to note that a large potential drop is produced at the edge of the domain in the quasi-neutral region between the center of the end-plug and the magnetic throat at the edge of the domain. This potential drop accelerates ions in the quasi-neutral region up to speeds approaching the ion sound speed. This reduces the potential drop required at the sheath region to achieve ambipolarity.

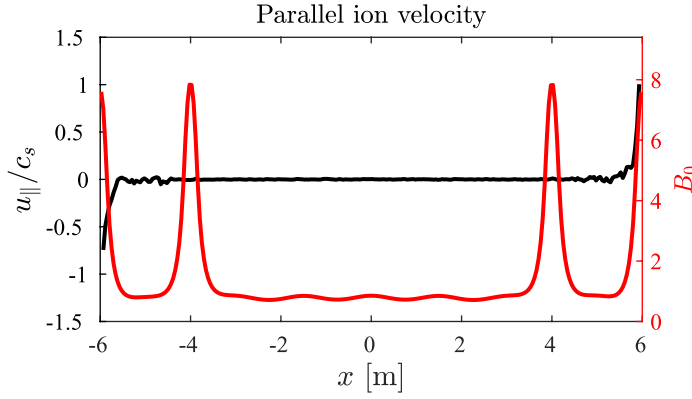


FIGURE 6. Parallel ion velocity (black) and magnetic field strength (red) along the length of the device. The electron temperature is taken to be uniform at a value of 1 keV.

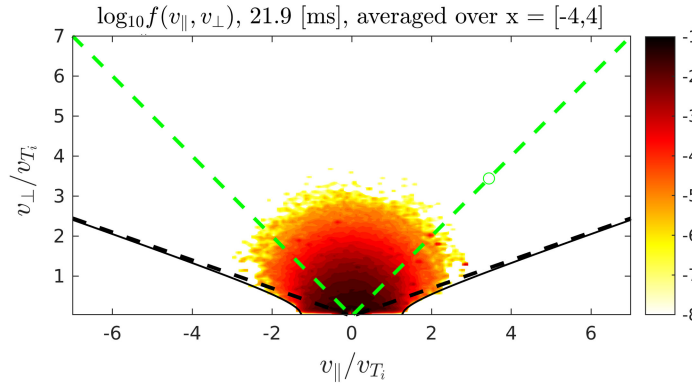


FIGURE 7. Ion distribution function in the central cell averaged over region  $-4$  to  $+4$  m at 21.9 ms. The black dotted and solid lines represent the trapped-passing boundary without and with the effect of the electrostatic potential respectively. The solid line indicates that a fraction of the low energy thermal ions is effectively confined by the electrostatic potential between the central cell and the end-plug as shown in figure 4. The NBI energy in each end-plug is 25 keV at 0.4 MW.

The ion distribution function in the central cell in figure 7 is assembled by integrating the region  $x_m = -4$  to  $+4$  m. The black solid line represents the trapped-passing boundary with the effect of the electric potential given by (3.6), where  $\Delta V$  is the potential difference between the central cell and the maximum potential in the end-plug at  $x = 5$  m. Due to the sign of the potential (positive), the trapped-passing boundary crosses the horizontal axis at values of  $v_{\parallel} = \pm \sqrt{2e\Delta V/M}$ . If we normalize this quantity by a characteristic ion thermal velocity  $v_T = \sqrt{2eT/M}$  we get  $v_{\parallel}/v_T = \pm \sqrt{\Delta V/T}$  which defines the region in velocity space confined by the electrostatic potential. Given the potential difference  $\Delta V \approx 1.7$  keV between the central cell and end-plug and an ion temperature in that region of about 1 keV, we get  $v_{\parallel}/v_T = 1.28$ .

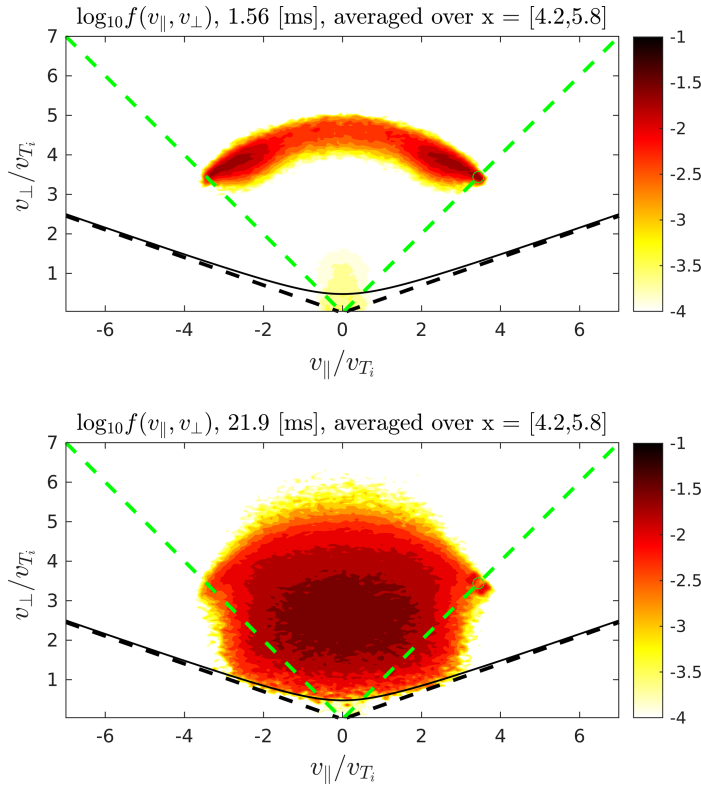


FIGURE 8. Ion distribution function in the end-plugs at 1.56 ms (top) and 21.9 ms (bottom) averaged over region  $x_m = 5m \pm 0.8m$ . The black solid and dotted lines represent the trapped-passing boundary with and without the effect of the electrostatic potential, respectively. The green dotted lines represent the NBI injection angle (45 degrees). The NBI energy in each end-plug is 25 keV and power is 0.4 MW.

$$v_{\parallel}^2 = v_{\perp}^2 (R - 1) + \frac{2e\Delta V}{M} \quad (3.6)$$

The distribution function in the end-plugs is shown in figure 8. The top shows the sloshing ions at early times. The black solid line represents the trapped-passing boundary with the effect of the electrostatic potential given by (3.6). In this case, the potential difference is between the end-plug maximum and the throat at the edge of the domain. It is negative and accelerates low energy ions out of the end-plug. This empties the low energy portion of the distribution function which is re-populated via collisional diffusion from the confined region. Everything above the hyperbolic trapped-passing boundary is confined (electrostatic and magnetic) in the end-plugs.

### 3.3. 100 keV beam case

This case is identical to the previous case except 100 keV beams are used. Neutral beams are injected into the end-plugs at 45 degrees relative to the magnetic field as per table 1 from the start of the simulation. This case is evolved up to 23 ms, less than the thermalization time. The electron density profile at various time steps

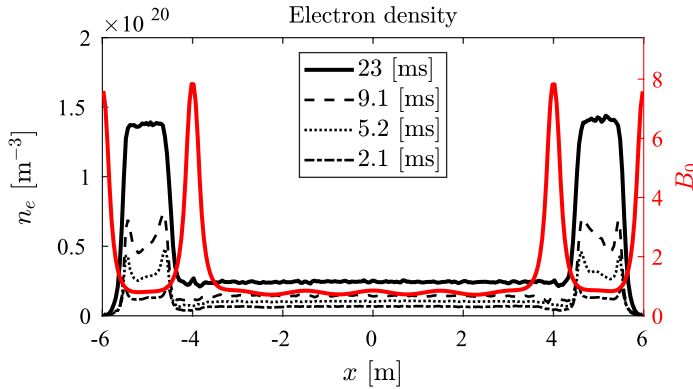


FIGURE 9. Electron density (black) along the length of the device for various simulation times (see legend). The magnetic field strength along the length of the computational domain is represented by the red trace. The NBI energy in each end-plug is 100 keV at 0.4 MW.

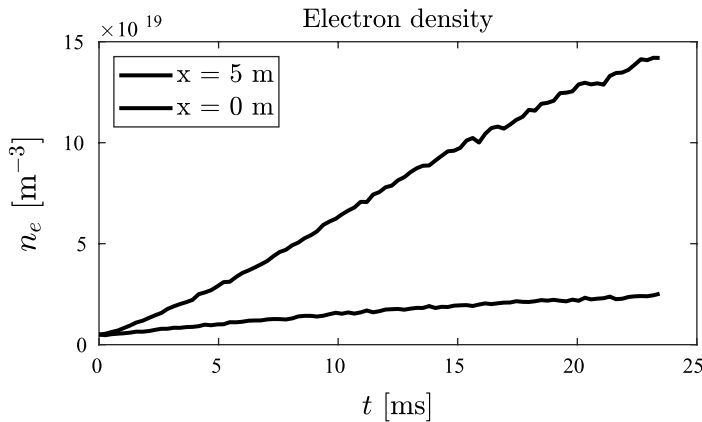


FIGURE 10. Electron density temporal evolution in the central cell (dashed) and end-plug (solid) region. The NBI energy in each end-plug is 100 keV at 0.4 MW.

is presented in [figure 9](#). Temporal evolution in the end-plugs ( $x = 5$  m) and in the central cell ( $x = 0$  m) is shown in [figure 10](#).

Temporal evolution of the ion temperature in the end-plugs is shown in [figure 11](#). Perpendicular temperature is close to the injection energy of 100 keV and remains steady up to about 15 ms and then starts to drop indicating the beginning of the thermalization process.

The electric potential associated with the plasma density profile in [figure 9](#) at 23 ms is presented in [figure 12](#) below. Despite the higher NBI energy (100 keV), the potential difference between the central cell and the end-plugs is approximately  $1.8T_e$  or 1.8 keV which is only slightly higher than in the 25 keV case. How this happens remains unclear. We speculate that the use of a fully non-linear Fokker-Planck collision operator including the electrons will modify this result. As the beam slows down, it heats the electrons and this in turn reduces the drag on the fast

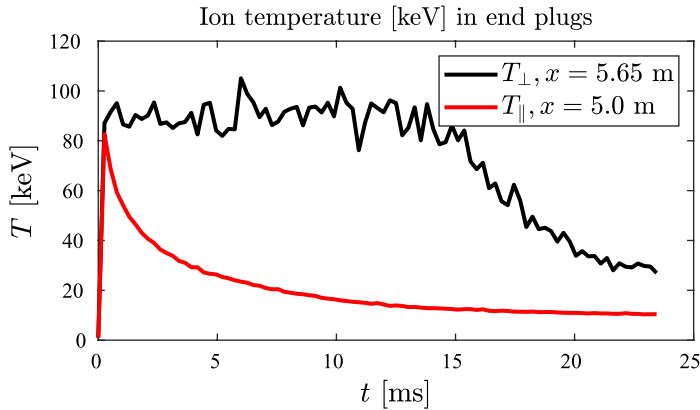


FIGURE 11. Parallel (red) and perpendicular (black) ion temperatures in the end-plugs. The perpendicular and parallel temperature is taken at the turning point of the sloshing ions density and mid plane of end-plugs respectively. The NBI energy in each end-plug is 100 keV at 0.4 MW.

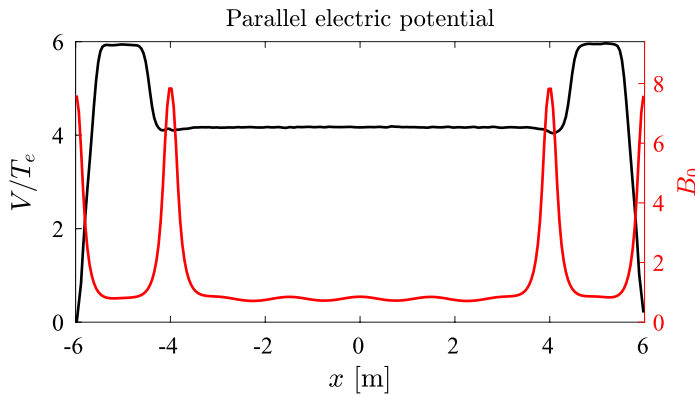


FIGURE 12. Parallel electric potential (black) and magnetic field strength (red) along the length of the device. The electron temperature is taken to be uniform at a value of 1 keV. The NBI energy in each end-plug is 100 keV at 0.4 MW.

ions on electrons thus increasing the confinement of the beam and the sloshing ion density. The increased end-plug density would increase the potential difference. The ion distribution function in the central cell for this 100 keV case looks very similar to that presented in figure 8 except for the small change in the trapped-passing boundary intercept where  $v_{\parallel}/v_T = 1.33$ .

### 3.4. Effect of the end-plug electron temperature

In this section, we investigate the effect of increasing the end-plug electron temperature ( $T_{ep}$ ) relative to that in the central cell ( $T_{ec}$ ) on the electric potential and the central cell confinement.

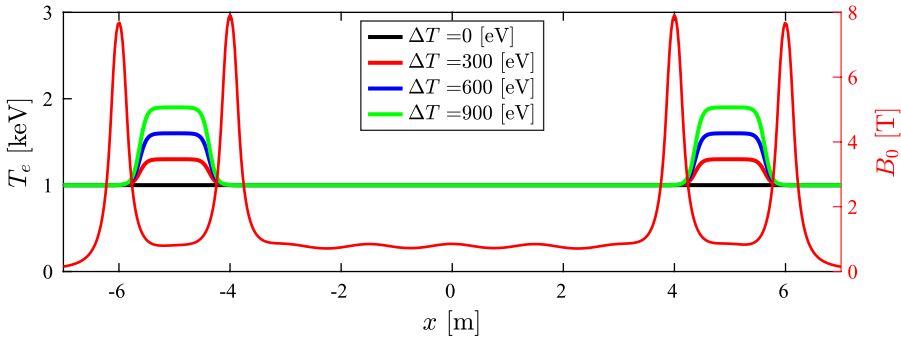


FIGURE 13. Electron temperature profiles where the value at the end-plugs is systematically increased to observe the effect on confinement and electrostatic potential.

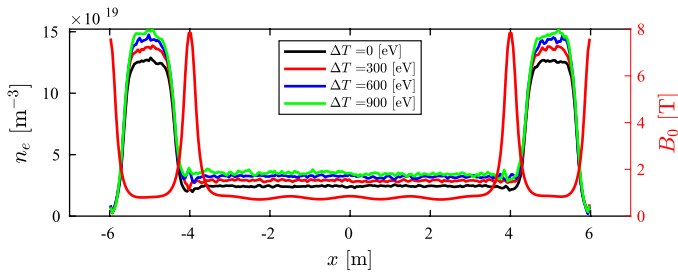


FIGURE 14. Electron density profiles at the end of the simulation (22 ms) for the various electron temperature profiles presented in Figure 13.

### 3.4.1. Numerical results

PICOS++ simulations were performed with 25 keV NBI as per the conditions in table 1; however, a new feature was introduced: the electron temperature in the end-plugs was systematically increased while keeping the central cell electron temperature the same at 1 keV as illustrated in figure 13. The electron density profiles along the length of the computational domain at the end of the simulations (22 ms) for the different electron temperature scenarios are presented in figure 14. The associated electric potential profiles are presented in figure 15. The results show an increase in density in both the central cell and end-plugs. The increase in density in the end-plugs is likely caused by the reduced electron drag on the sloshing ions. The increase in density in the central cell is caused by the improved confinement time in connection with increased end-plug potentials. In § 3.4.3, the observed confinement times are compared with those predicted by the Pastukhov expression (3.1).

### 3.4.2. Electric potential scaling with temperature

To understand the effect of electron temperature differences between the central cell and the end-plugs on the formation of the electric potential, we present a simple model (B5) in Appendix B.

In this section, we compare the observed potentials with those predicted by such model. This expression (B5) is composed of two terms: (1) the first term is the

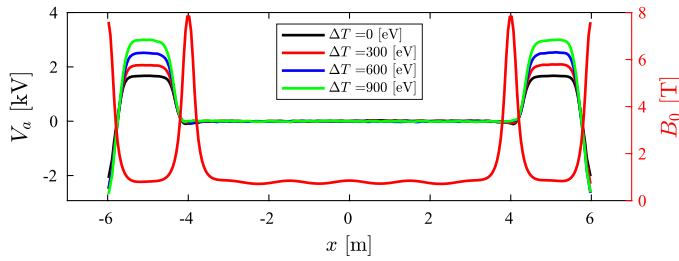


FIGURE 15. Parallel electric potential profiles at the end of the simulation (22 ms) for the various electron temperature profiles presented in Figure 13.

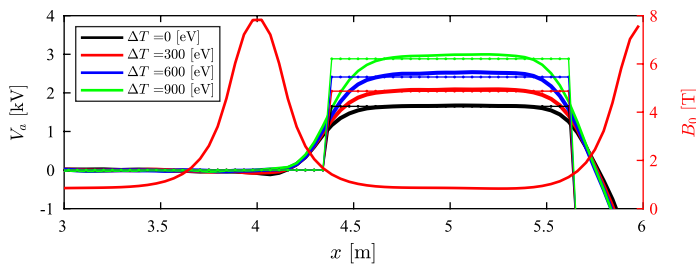


FIGURE 16. Comparing the electric potential profiles from PICOS (solid lines) and those predicted by (A1) (dotted lines) at the end of the simulation (22 ms) for the various electron temperature profiles presented in figure 13.

standard Boltzmann response which scales with  $\log(n_{ep}/n_{ec})$ , where  $n_{ep}$  and  $n_{ec}$  represent the electron density in the end-plug and central cell respectively; (2) the second term describes the effect of having an electron temperature difference  $\Delta T_e$  between the central cell and end-plug and scales *linearly* with  $\Delta T_e$ . In figure 16, the observed potential differences (solid lines) are compared with those predicted by (B5) (dotted lines). Equation (B5) was evaluated by approximating the electron temperature profiles (figure 13) and electron density profiles (figure 14) with Heaviside step functions. The results show that the jump in potential between central cell and the end-plug is well described by the simple expression provided in (B5) using the Heaviside approximation; namely, the potential difference scales *linearly* with  $\Delta T_e$ .

### 3.4.3. Confinement time

Finally, the confinement time observed numerically is compared with the confinement time predicted by the Pastukhov expression in (3.1). The results are presented in figure 17. The observed confinement time is obtained by fitting (3.4) to the time-dependent central cell density produced by PICOS++. For this comparison, we provide an upper and lower bound on the fitted confinement time. The theoretical confinement time (3.1) is evaluated and averaged during the steady-state period of the end-plug density ( $t > 14$  ms). The comparison presented in figure 17 indicates that both the observed and theoretical confinement times are consistent and have similar scaling with respect to the normalized potential difference  $\Delta V/T_e$ ; however, at the larger potential values the numerical results appear to overestimate theoretical



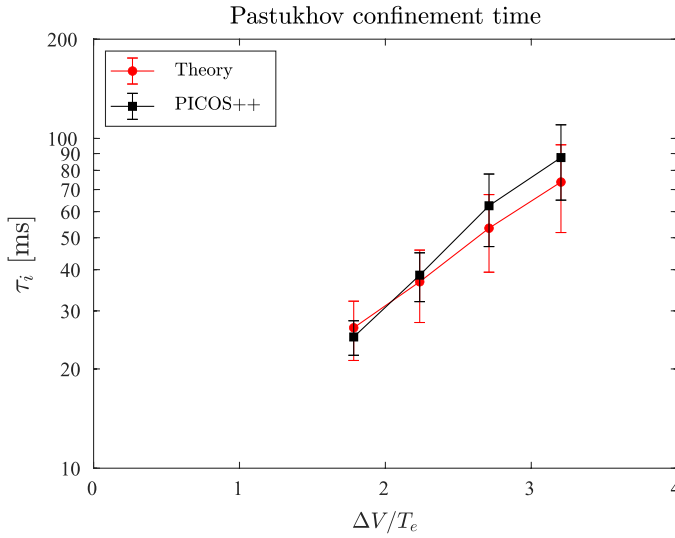


FIGURE 17. Comparing the numerically observed confinement times (black squares) and those predicted by (1.9) (red circles) for the various electron temperature profiles presented in figure 13.

predictions, where the observed and predicted mean confinement times are 87 ms and 73 ms respectively. A more detailed and in-depth comparison would require running the numerical simulations to full steady-state so that the confinement time values are extracted directly from the steady-state central cell density rather than fitting the time-dependent part. This will be the subject of a future study.

#### 4. Discussion

Previous work on mirror device modeling presented in reference (Endrizzi *et al.* 2023) makes use of the Bounce-Averaged (BA) solution of the Fokker-Planck (FP) equation using the CQL3D-m code. CQL3D-m is derived from the well-established tokamak-specific CQL3D code and adapted to mirror geometry. A key advantage of the BA formulation is that simulated times in the order of seconds are computationally readily accessible; however, in its current form, this formulation is only applicable to simple mirrors. Extensions to multiple mirror geometries such as tandem mirrors are at present being explored in CQL3D-m but not fully developed.

In this work, we demonstrate that PICOS++ can seamlessly model scenarios with multiple mirrors since the ion dynamics and associated distribution function are followed along the magnetic flux, without complications such as multiple mirror regions in CQL3D-m. In its present form, PICOS++ readily captures essential features of the tandem mirror concept; namely, electrostatic confinement of the central cell low energy ions via beam-driven, high-density, magnetically confined end-plugs. Moreover, the results from PICOS++ are consistent with the analytical expressions for the Pastukhov confinement time. However, an important limitation in the present form of PICOS++ is the lack of a fully non-linear Fokker-Planck Monte-Carlo (FPMC) collision operator. This limitation is most clearly observed when forming beam-driven sloshing ion distributions in the end-plugs. The effect of highly non-thermal distribution is not captured by the linearized Fokker-Planck operator

currently in place. Incorporating a fully non-linear FP Monte-Carlo collision operation in PICOS++ is currently in progress and based on references (Wang *et al.* 1995; Takizuka and Abe 1977). Once this is available, confinement/slowing down times and electric potential profile calculations can be compared with analytical expressions and results from other codes.

The next logical actions to improve the predictive capability of the code are the following: (a) enable the fully non-linear FPMC collision operator to capture beam physics more accurately, (2) develop concentrically nested flux surface solutions to capture the radial variation of the plasma and (3) develop an exhaust region solution that can be linked to the confined region solutions. The second step described above will enable us to introduce a more physics-based NBI module which makes use of radial plasma profiles and models beam capture via charge-exchange and impact ionization and shine-through. The third step is necessary to capture the electrostatic confinement of electrons which stream out of the end-plugs. In the exhaust region, ions are accelerated in the expanding magnetic field lines by the electrostatic field, whereas the electric potential reflects electrons back into the confined plasma. With sufficient field line expansion, a large fraction of electrons is reflected back into the confined region before interacting at the wall-sheath region where the presence of neutral gas can lead to electron cooling. The need here is to develop an exhaust-expander solution for both ions and electrons and connect them via boundary conditions to the solutions in the confined region produced by PICOS++, CQL3D-m or other codes.

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### Declaration of interests

The authors report no conflict of interest.

### Appendix A.

The Monte-Carlo linearized FP collision operator used at present in PICOS++ (2.7) and (2.8) is compared with analytical expressions for the slowing down and cosine pitch angle scattering obtained from references (Hinton 1983; Boozer and Kuo-Petravic (1998). The velocity of a group of particles is evolved in time using the collision operator; however, the advance particle operator is not used. The initial value problem describing the slowing down of ions in a background plasma is given by (A1), where  $\nu^E$  is the slowing down rate given in (92) from reference (Hinton 1983). Equation (A1) describes the change in kinetic energy  $E$  of an ion as it interacts with a background species with fixed conditions described in table 2. The evolution of the mean cosine pitch angle  $\xi = \cos(\eta)$  is described by (A2). When the mean value of the cosine pitch angle reaches zero, it indicates that the expression is dominated by the stochastic term, any memory of the starting pitch angle is lost, and any pitch angle is equally likely. The comparison between the Monte-Carlo collision operator

MC collision operator parameters		Physical value
Total simulation time		25–60 ms
Electron temperature		1 keV
Electron density		$5 \times 10^{19} \text{ m}^{-3}$
Number of ion species		1
Ion species 1 mass number		2 AMU
Ion species 1, charge number		+1
Ion species 1, temperature		1 keV
Number of computational particles		25
Particle advance time step $\Delta t$		$0.5 \mu\text{s}$
Initial beam energy ( $E_0$ )		25 or 100 keV
Initial pitch angle ( $\eta_0$ )		45 degrees

TABLE 2. Simulation inputs used for the benchmarking of the collision operator with analytical expressions.

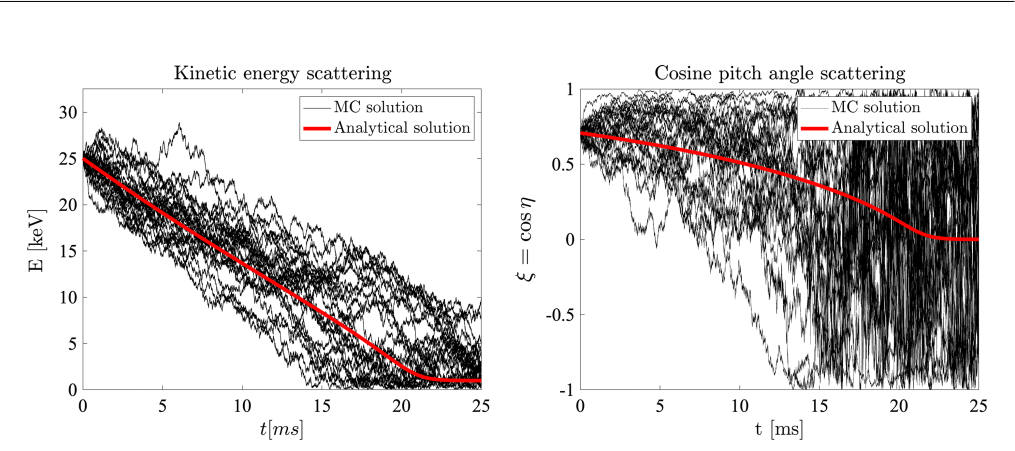


FIGURE 18. Temporal evolution of the kinetic energy (left) and cosine of pitch angle (right) of a 45 degree 25 keV beam. Monte–Carlo solution with both deterministic and stochastic part presented in black. Analytical solutions presented in red.

and the analytical expressions are provided in figures 18 and 19 for the 25 keV and 100 keV case respectively.

$$\frac{dE}{dt} + v^E E = 0 \tag{A1}$$

$$\frac{d\xi}{dt} + v^D \xi = 0 \tag{A2}$$

**Appendix B.**

The starting point for deriving the electric field in a quasi-neutral plasma with isotropic but non-uniform profiles is to use equation (2.6). In the case of a uniform electron temperature  $T_e$ , the electric potential between the central cell and

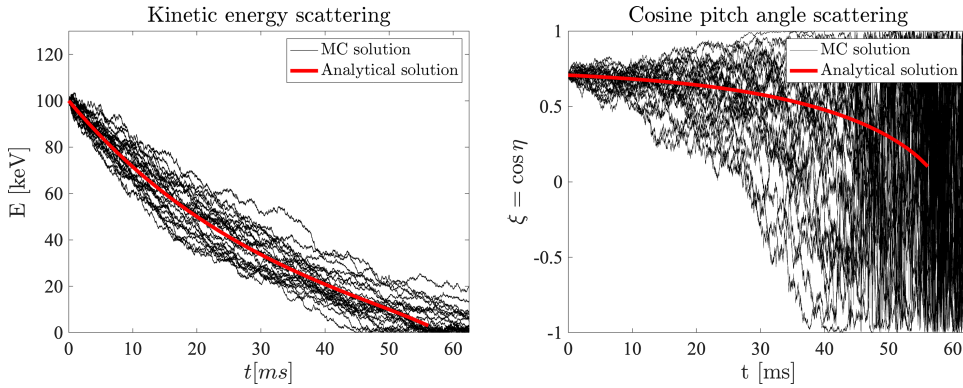


FIGURE 19. Temporal evolution of the kinetic energy (left) and cosine of pitch angle (right) of a 45 degree 100 keV beam. Monte–Carlo solution with both deterministic and stochastic part presented in black. Analytical solutions presented in red.

the end-plug takes the form of the so-called Boltzmann relation (B1) where  $n_{ep}$  and  $n_{ec}$  represent the electron density in the end-plug and central cell respectively. Under these circumstances, the potential difference scales linearly with  $T_e$  and logarithmically with the ratio of densities.

$$\Delta V(x) = T_e \ln\left(\frac{n_{ep}}{n_{ec}}\right) \quad (\text{B1})$$

What happens when we also have an electron temperature difference  $\Delta T_e$  between the central cell and end-plug? Can we derive a simple expression to understand the impact of  $\Delta T_e$  on the potential? To answer this, we derive a simple expression relating the electron temperature and density to the potential difference by approximating the profiles with Heaviside step functions. This approximation appears to be suitable considering the step-like profiles produced by PICOS++ and presented in figures 1 and 9. The numerical results demonstrate a step-like transition between the central cell and end-plugs.

We describe the electron temperature and density profiles with (B2) and (B3) respectively, where  $T_{ec}$  represents the electron temperature in the central cell,  $T_{ep}$  the electron temperature in the end-plug and  $\Delta T_e = T_{ep} - T_{ec}$ . The term  $x_1$  is the locations where  $T_e$  jumps from  $T_{ec}$  to  $T_{ep}$ ,  $x_2$  where it jumps from  $T_{ep}$  to  $T_{ec}$  and  $H(x)$  the Heaviside step function.

$$T_e(x) = T_{ec} + \Delta T_e(H(x - x_1) - H(x - x_2)) \text{ for } x > 0 \quad (\text{B2})$$

$$n_e(x) = n_{ec} + \Delta n_e(H(x - x_1) - H(x - x_2)) \text{ for } x > 0 \quad (\text{B3})$$

Taking the electron temperature to be isotropic but non-uniform, the parallel electric field is given by (2.6). Integrating the electric field and using integration by parts, the associated potential difference can be written as in (B4). Replacing the electron temperature with the Heaviside approximation (B2), we arrive at the piecewise expression in (B5) where  $n_e^* = n_e(x_1)$  is the electron density at the location where

$T_e$  transitions from  $T_{ec}$  to  $T_{ep}$ . If we broaden the density profile at the transition location, we can approximate  $n_e^* = n_e(x_1) \approx (n_{ec} + n_{ep})/2$ . Equation (B5) indicates the potential difference scales linearly with the temperature difference  $\Delta T_e$  and logarithmically with the density. When  $T_e$  becomes uniform, we recover the Boltzmann response for the potential ( $\Delta V = T_e \ln(n_{ep}/n_{ec})$ ).

$$\Delta V(x) = T_e|_0^x + T_e \ln n|_0^x - \int_0^x \ln n \frac{\partial T_e}{\partial s} ds \quad (\text{B4})$$

$$\Delta V(x) = \begin{cases} 0 & \text{for } x < x_1 \\ T_{ec} \ln\left(\frac{n_{ep}}{n_{ec}}\right) + \Delta T_e \left(1 + \ln\left(\frac{n_{ep}}{n_e^*}\right)\right); & \text{for } x_1 \leq x < x_2; n_e^* \approx \frac{n_{ep} + n_{ec}}{2} \\ 0 & \text{for } x \geq x_2 \end{cases} \quad (\text{B5})$$

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