

Revisiting Townsend's spatial energy-density function

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Fourier analysis is the standard tool of choice for quantifying the distribution of kinetic energy amongst the eddies in a turbulent flow. The resulting spectral energy-density function is the well-known energy spectrum. And yet, because eddies are distinct from waves, alternative approaches to finding energy-density functions have long been sought. Townsend (1976) outlined a promising approach to finding a spatial energy-density function, $V(r)$, where r is the eddy size. Notably, this approach led to two distinct and mutually inconsistent formulations of $V(r)$ in homogeneous, isotropic turbulence. We revisit Townsend's proposal and derive the corresponding three-dimensional $V(r)$ as well as introduce its one-dimensional variants (which, to our knowledge, have not been explicitly discussed before). By training our focus on the associated dimensionality of the function, we resolve the discrepancies between the previous formulations. Additionally, we generalise our analysis to include anisotropic flows. Finally, by means of concrete examples, we illustrate how one-dimensional spatial energy-density functions are useful for analysing empirical data. Some notable findings include new insights into the k_1^{-1} scaling (where k_1 is the streamwise wavenumber) and a possible resolution of the enigmatic sizes of organised motions at large scales.

Key words: isotropic turbulence, turbulence theory

1. Introduction

Turbulence is composed of blobs of fluid, called eddies, over which velocity fluctuations are highly correlated. These eddies span a broad range of sizes, and the distribution of turbulent kinetic energy across the range of eddy sizes is a critical attribute of a turbulent flow. We focus on the following question: How do we quantify this energy distribution? In other words, we need an energy-density function.

The standard approach to quantifying the distribution of energy is to introduce the spectral tensor, $\Phi_{ij}(\mathbf{k})$, which is the Fourier transform of the two-point velocity correlation tensor $Q_{ij}(\mathbf{r}) := \langle u_i(\mathbf{x})u_j(\mathbf{x} + \mathbf{r}) \rangle$

$$\Phi_{ij}(\mathbf{k}) = \frac{1}{(2\pi)^3} \int_{\mathbb{R}^3} d^3\mathbf{r} Q_{ij}(\mathbf{r}) e^{-i\mathbf{k} \cdot \mathbf{r}}, \quad (1.1a)$$

$$Q_{ij}(\mathbf{r}) = \int_{\mathbb{R}^3} d^3\mathbf{k} \Phi_{ij}(\mathbf{k}) e^{i\mathbf{k} \cdot \mathbf{r}}, \quad (1.1b)$$

where \mathbf{x} and $\mathbf{x} + \mathbf{r}$ are position vectors, \mathbf{k} is the wavenumber corresponding to \mathbf{r} , \mathbf{u} is the turbulent velocity vector, the subscript indices denote Cartesian components of the corresponding vector or tensor and $\langle \rangle$ denotes an ensemble average. Note that we have assumed the turbulent flow to be homogeneous (i.e. its statistical properties are independent of \mathbf{x}). In this study, we shall restrict attention to homogeneous turbulence. When the turbulent flow is homogeneous and isotropic, we can introduce the three-dimensional spectral energy-density function, $E(k)$, by integrating $(1/2)\Phi_{ii}(\mathbf{k})$ over a spherical shell, $\mathcal{S}(k)$, of radius $k = \|\mathbf{k}\|$

$$E(k) := \oint \frac{1}{2} \Phi_{ii}(\mathbf{k}) d\mathcal{S}(k). \quad (1.2)$$

The factor of $1/2$ was introduced to obtain the energy constraint

$$\frac{1}{2} \langle \mathbf{u}^2 \rangle = \int_0^\infty dk E(k), \quad (1.3)$$

which follows from (1.1b) and the relations $Q_{ii}(r=0) = \langle \mathbf{u}^2 \rangle$ and $Q_{ii}(r \rightarrow \infty) = 0$, where $r = \|\mathbf{r}\|$. (For simplicity of notation, in this study, we use the same symbol to represent a function whether its argument is a vector, e.g. \mathbf{r} , or its scalar norm, r). The energy constraint underpins the role of $E(k)$ as an energy-density function. Specifically, it implies that $dk E(k)$ is the contribution to $(1/2)\langle \mathbf{u}^2 \rangle$ (which is the turbulent kinetic energy) from wavenumber modes in the range $(k, k + dk)$ so that the function $E(k)$ represents the energy density in the spectral space. But the problem here is how to interpret k in terms of eddies. Although, as a rule of thumb, we may loosely associate k^{-1} with the eddy size, because eddies are not waves, the validity of such one-to-one association is unclear.

These difficulties underscore the need for a complementary approach; see Davidson (2004, Ch. 6) for a detailed discussion of this topic. In the real space, the analogue of $E(k)$ is a spatial energy-density function, $V(r)$. In analogy with the properties of $E(k)$, we can require $V(r)$ to have the following characteristic properties (Davidson 2004):

- (i) $V(r) \geq 0$;
- (ii) $\int_0^\infty dr V(r) = (1/2)\langle \mathbf{u}^2 \rangle$;
- (iii) for a random distribution of eddies of fixed size ℓ_e , the corresponding $V(r)$ manifests a clear peak around $r \sim \ell_e$.

An insightful approach to obtain $V(r)$ was pioneered by Townsend (1976). Unlike the case in the spectral space, where linking k^{-1} with eddy size is unclear, he sought to construct a function in the real space whose magnitude for the argument r is clearly related to the energy of eddies of ‘diameter’ r . For that purpose, he used Kolmogorov’s two-point velocity structure function (Kolmogorov 1941)

$$S_{ij}(\mathbf{r}) := \langle [u_i(\mathbf{x}) - u_i(\mathbf{x} + \mathbf{r})][u_j(\mathbf{x}) - u_j(\mathbf{x} + \mathbf{r})] \rangle. \quad (1.4)$$

Consider the velocity component directed along $\mathbf{r} = r\hat{\mathbf{e}}_1$. Heuristically, it is argued that $S_{11}(r)$ is dominated by contributions from eddies of size r or less. This is because eddies of size r or greater make comparable contributions to both $u_1(\mathbf{x})$ and $u_1(\mathbf{x} + \mathbf{r})$, and thus contribute little to $S_{11}(r)$. With this picture in mind, he postulated that the contribution to $\langle u_1^2 \rangle$ from eddies of size r in unit range of $\log r$ is

$$-r \frac{\partial}{\partial r} \left[\frac{1}{2} S_{11}(r) \right]. \quad (1.5)$$

Notably, Townsend did not obtain an explicit expression for $V(r)$ from (1.5). That task was taken up only relatively recently.

Davidson (2004) argued that Townsend's proposal leads to

$$V_{TD}(r) := \frac{\partial}{\partial r} \left[\frac{3}{4} \langle [\Delta v(r)]^2 \rangle \right], \quad (1.6)$$

where $\langle [\Delta v(r)]^2 \rangle$ is the longitudinal structure function, which is defined as

$$\langle [\Delta v(r)]^2 \rangle := S_{ij} \frac{r_i r_j}{r^2}. \quad (1.7)$$

We shall refer to $V_{TD}(r)$ as the Townsend–Davidson function. On the other hand, Hamba (2015) postulated

$$V_{TH}(r) := -\frac{\partial}{\partial r} \frac{1}{2} Q_{ii}(r), \quad (1.8)$$

which we shall refer to as the Townsend–Hamba function. (Note that $V_{TH}(r)$ is closely related to equation (13) of Danaila, Antonia & Burattini (2012).) Surprisingly, although they stem from the same proposal, the expressions for $V_{TD}(r)$ and $V_{TH}(r)$ are distinct.

Inspired by Davidson (2004) and Hamba (2015), we take a fresh look at deriving $V(r)$. We first discuss homogeneous isotropic turbulence, and then generalise our approach to anisotropic flows. Thereafter, we draw attention to an important point that has not been explicitly considered before. Analogous to the well-known one-dimensional spectral energy-density functions, we introduce one-dimensional spatial energy-density functions. This allows us to resolve the surprising discrepancies between (1.6) and (1.8). Moreover, the one-dimensional functions may find particular appeal for the analysis of empirical data. We demonstrate this point with a few illustrative examples.

2. Deriving $V(r)$ for homogeneous isotropic turbulence

In the spectral space, the energy constraint of (1.3) underpins the interpretation of $E(k)$ as an energy-density function. Here, we derive $V(r)$ for homogeneous isotropic turbulence using a spatial analogue of the energy constraint. (In Appendix A, we derive this expression using Townsend's approach).

From the sifting property of the Dirac delta function $\delta(r)$, we can write

$$\frac{1}{2} Q_{ii}(r) = \int_0^\infty dr' \left[\frac{1}{2} Q_{ii}(r') \right] \delta(r' - r). \quad (2.1)$$

By introducing the Heaviside function $\Theta(r)$, the above integral can be expressed as

$$\begin{aligned}
 \frac{1}{2} Q_{ii}(r) &= \int_0^\infty dr' \left[\frac{1}{2} Q_{ii}(r') \right] \frac{\partial}{\partial r'} \Theta(r' - r), \\
 &= \int_0^\infty dr' \frac{\partial}{\partial r'} \left[-\frac{1}{2} Q_{ii}(r') \right] \Theta(r' - r), \quad (\text{integration by parts}) \\
 &= \int_r^\infty dr' \frac{\partial}{\partial r'} \left[-\frac{1}{2} Q_{ii}(r') \right],
 \end{aligned} \tag{2.2}$$

where we have used $Q_{ii}(r \rightarrow \infty) = 0$. Taking the limit $r \rightarrow 0$ and noting $Q_{ii}(0) = \langle \mathbf{u}^2 \rangle$, we have

$$\int_0^\infty dr' \left[-\frac{\partial}{\partial r'} \frac{1}{2} Q_{ii}(r') \right] = \frac{1}{2} \langle \mathbf{u}^2 \rangle, \tag{2.3}$$

which is a real-space analogue of the spectral-space energy constraint, (1.3). Thus, analogous to the three-dimensional spectral energy-density function, $E(k)$, we can define a three-dimensional spatial energy-density function

$$V(r) := -\frac{\partial}{\partial r} \frac{1}{2} Q_{ii}(r), \tag{2.4}$$

which is the Townsend–Hamba function, $V_{TH}(r)$ (1.8).

Some additional remarks may be useful. Although we could have derived (2.4) without (2.2), introducing (2.2) allows us to interpret $Q_{ii}(r)$ in terms of kinetic energy of eddies. Combining (2.2) and (2.4), we get

$$\frac{1}{2} Q_{ii}(r) = \int_r^\infty ds V(s) = \int_0^\infty ds V(s) \Theta(s - r). \tag{2.5}$$

Here, the ideal low-pass filter $\Theta(r)$ ensures that only eddies of size r or greater make contributions to $(1/2)Q_{ii}(r)$, with the implication

$$\frac{1}{2} Q_{ii}(r) = [\text{cumulative kinetic energy held in eddies of size } r \text{ or greater}]. \tag{2.6}$$

This interpretation based on $V(r)$ can be contrasted with that based on $E(k)$. We can express $Q_{ii}(r)$ in terms of $E(k)$ as

$$\frac{1}{2} Q_{ii}(r) = \int_0^\infty dk E(k) \frac{\sin(kr)}{kr}. \tag{2.7}$$

Note that, while $\sin(kr)/(kr)$ effectively is a low pass-filter, dominated by contributions from wavenumbers $k \lesssim 1/r$, it is not an ideal filter and has an infinite extent in k -space. Thus, all Fourier modes contribute to $(1/2)Q_{ii}(r)$. Interpreting the Fourier modes as eddy sizes implies that eddies of all sizes contribute to $(1/2)Q_{ii}(r)$. The above discussion underscores how different definitions of the energy-density function embody distinct physical interpretations; also see Davidson (2004).

3. Deriving $V(r)$ for homogeneous anisotropic turbulence

So far, we have focused on homogeneous isotropic turbulence. Next we generalise the analysis of § 2 for homogeneous anisotropic turbulence and derive an expression for the three-dimensional spatial energy-density function, $V(\mathbf{r})$.

We begin with extending (2.1) for the general case (without assuming isotropy or homogeneity)

$$\frac{1}{2} Q_{ii}(\mathbf{r}, \mathbf{x}) = \int_{\Omega} d^3 \mathbf{r}' \left[\frac{1}{2} Q_{ii}(\mathbf{r}', \mathbf{x}) \right] \delta^3(\mathbf{r}' - \mathbf{r}), \quad (3.1)$$

where Ω is any arbitrary flow domain (with the restriction that \mathbf{r} is contained within it) and $\delta^3(\mathbf{r})$ denotes the Dirac delta function in \mathbb{R}^3 . Noting that the Dirac delta function satisfies the relation

$$\nabla \cdot \left[\left(\frac{1}{4\pi} \frac{\mathbf{r} - \mathbf{r}'}{||\mathbf{r} - \mathbf{r}'||^3} \right) \right] = \delta^3(\mathbf{r} - \mathbf{r}'), \quad (3.2)$$

we write (3.1) as

$$\begin{aligned} \frac{1}{2} Q_{ii}(\mathbf{r}, \mathbf{x}) &= \int_{\Omega} d^3 \mathbf{r}' \nabla' \cdot \left[\frac{1}{2} Q_{ii}(\mathbf{r}', \mathbf{x}) \frac{1}{4\pi} \frac{\mathbf{r}' - \mathbf{r}}{||\mathbf{r}' - \mathbf{r}||^3} \right] \\ &\quad - \int_{\Omega} d^3 \mathbf{r}' \frac{1}{4\pi} \frac{\mathbf{r}' - \mathbf{r}}{||\mathbf{r}' - \mathbf{r}||^3} \cdot \nabla' \left[\frac{1}{2} Q_{ii}(\mathbf{r}', \mathbf{x}) \right]. \end{aligned} \quad (3.3)$$

Applying the divergence theorem yields

$$\begin{aligned} \frac{1}{2} Q_{ii}(\mathbf{r}, \mathbf{x}) &= \int_{\partial\Omega} dS \frac{1}{2} Q_{ii}(\mathbf{r}', \mathbf{x}) \frac{1}{4\pi} \frac{(\mathbf{r}' - \mathbf{r}) \cdot \mathbf{n}'}{||\mathbf{r}' - \mathbf{r}||^3} \\ &\quad - \int_{\Omega} d^3 \mathbf{r}' \frac{1}{4\pi} \frac{\mathbf{r}' - \mathbf{r}}{||\mathbf{r}' - \mathbf{r}||^3} \cdot \nabla' \left[\frac{1}{2} Q_{ii}(\mathbf{r}', \mathbf{x}) \right], \end{aligned} \quad (3.4)$$

where \mathbf{n}' is the unit normal to the surface $\partial\Omega$ that bounds the domain Ω . This brings us to a critical consideration. When the turbulence is homogeneous, the surface integral in (3.4) vanishes, yielding

$$\frac{1}{2} Q_{ii}(\mathbf{r}) = \int_{\Omega} d^3 \mathbf{r}' \frac{1}{4\pi} \frac{\mathbf{r}' - \mathbf{r}}{||\mathbf{r}' - \mathbf{r}||^3} \cdot \nabla' \left[-\frac{1}{2} Q_{ii}(\mathbf{r}') \right]. \quad (3.5)$$

This is the generalisation of (2.2) for homogeneous anisotropic turbulence.

Next, taking the limit $\mathbf{r} \rightarrow \mathbf{0}$, we arrive at the energy constraint

$$\int_{\Omega} d^3 \mathbf{r}' \frac{1}{4\pi} \frac{1}{||\mathbf{r}'||^2} \hat{\mathbf{r}}' \cdot \nabla' \left[-\frac{1}{2} Q_{ii}(\mathbf{r}') \right] = \frac{1}{2} \langle \mathbf{u}^2 \rangle, \quad (3.6)$$

where we have used $Q_{ii}(\mathbf{0})/2 = \langle \mathbf{u}^2 \rangle/2$ and $\hat{\mathbf{r}}' := \mathbf{r}'/||\mathbf{r}'||$. From (3.6), we can define a three-dimensional spatial energy-density function

$$V(\mathbf{r}) := \frac{1}{4\pi} \frac{1}{||\mathbf{r}||^2} \hat{\mathbf{r}} \cdot \nabla \left[-\frac{1}{2} Q_{ii}(\mathbf{r}) \right] = \frac{1}{4\pi ||\mathbf{r}||^2} D_{\mathbf{r}} \left[-\frac{1}{2} Q_{ii}(\mathbf{r}) \right], \quad (3.7)$$

where $D_{\mathbf{r}} := \hat{\mathbf{r}} \cdot \nabla$ is the directional derivative. For the case of homogeneous isotropic turbulence, we can simplify (3.7) by averaging $V(\mathbf{r})$ over a spherical shell $S(r)$, $\oint_{S(r)} V(\mathbf{r}) dS(r)$, similar to the definition of $E(k)$ (cf. (1.2)). This transforms (3.7) to (2.4), thereby verifying self-consistency of the derivation discussed here.

Can the above analysis be readily generalised for inhomogeneous turbulence? For example, we may expect that (3.7) simply generalises to (cf. (18) in Hamba 2015)

$$V(\mathbf{x}, \mathbf{r}) := \frac{1}{4\pi ||\mathbf{r}||^2} D_{\mathbf{r}} \left[-\frac{1}{2} Q_{ii}(\mathbf{x}, \mathbf{r}) \right]. \quad (3.8)$$

We urge caution with this step. As we noted in the discussion of (3.4), the surface integral vanishes for homogeneous turbulence. But that may not hold for inhomogeneous turbulence. Note, however, that for the case of inhomogeneous turbulence where there exists one or more directions of homogeneity (e.g. streamwise and azimuthal directions in a fully developed pipe flow), the surface integral still vanishes when \mathbf{r} is restricted to the homogeneous directions.

4. One-dimensional spatial energy-density functions

In the analysis so far, we considered the three-dimensional spatial energy-density function. Here, we turn attention to the corresponding one-dimensional functions. In the spectral space, one-dimensional spectral energy-density functions, typically denoted by $E_{11}(k_1)$, $E_{22}(k_1)$, \dots , are well known (Davidson 2004). They are particularly useful in the analysis of experimental data, wherein measuring the (three-dimensional) $E(k)$ is very challenging. In the same spirit, here we seek to derive one-dimensional spatial energy-density functions.

For a homogeneous anisotropic turbulent flow, consider the direction $\mathbf{r} = r_1 \hat{\mathbf{e}}_1$. The associated longitudinal velocity correlation function can be expressed as (cf. (3.1))

$$\frac{1}{2} Q_{11}(r_1 \hat{\mathbf{e}}_1) = \int_0^\infty d\xi \left[\frac{1}{2} Q_{11}(\xi \hat{\mathbf{e}}_1) \right] \delta(\xi - r_1). \quad (4.1)$$

Following the analysis of § 2, we can simplify the above integral as

$$\frac{1}{2} Q_{11}(r_1 \hat{\mathbf{e}}_1) = \int_{r_1}^\infty d\xi \frac{\partial}{\partial \xi} \left[-\frac{1}{2} Q_{11}(\xi \hat{\mathbf{e}}_1) \right], \quad (4.2)$$

where we have used $Q_{11}(r_1 \rightarrow \infty) = 0$. Taking the limit $r_1 \rightarrow 0$ leads to an energy constraint

$$\int_0^\infty d\xi \left[-\frac{\partial}{\partial \xi} \frac{1}{2} Q_{11}(\xi \hat{\mathbf{e}}_1) \right] = \frac{1}{2} \langle u_1^2 \rangle, \quad (4.3)$$

where we have used $Q_{11}(\mathbf{0})/2 = \langle u_1^2 \rangle/2$. We can now define a (one-dimensional) longitudinal spatial energy-density function

$$V_{11}(r_1) := -\frac{\partial}{\partial r_1} \frac{1}{2} Q_{11}(r_1 \hat{\mathbf{e}}_1), \quad (4.4)$$

where $V_{11}(r_1) dr_1$ is the contribution to the turbulent energy component $(1/2) \langle u_1^2 \rangle$ from eddies of size in the range $(r_1, r_1 + dr_1)$.

Following the above procedure, we can define (one-dimensional) transverse spatial energy-density functions

$$V_{22}(r_1) := -\frac{\partial}{\partial r_1} \frac{1}{2} Q_{22}(r_1 \hat{\mathbf{e}}_1), \quad (4.5a)$$

$$V_{33}(r_1) := -\frac{\partial}{\partial r_1} \frac{1}{2} Q_{33}(r_1 \hat{\mathbf{e}}_1). \quad (4.5b)$$

These functions satisfy the corresponding energy constraints

$$\int_0^\infty dr_1 V_{22}(r_1) = \frac{1}{2} \langle u_2^2 \rangle, \quad (4.6a)$$

$$\int_0^\infty dr_1 V_{33}(r_1) = \frac{1}{2} \langle u_3^2 \rangle. \quad (4.6b)$$

(In [Appendix C](#), we discuss the relationship between the spectral and spatial variants of the one-dimensional energy-density functions.) Also note that the analysis discussed here can be easily extended to other directions, namely, $\mathbf{r} = r_2 \hat{\mathbf{e}}_2$ and $\mathbf{r} = r_3 \hat{\mathbf{e}}_3$. This yields one-dimensional spatial energy-density functions such as $V_{11}(r_2)$, $V_{11}(r_3)$, etc.

Last, we consider homogeneous isotropic turbulence. In this case, (4.4) and (4.5) transform to

$$V_{11}(r) := -\frac{\partial}{\partial r} \frac{1}{2} Q_{11}(r) = -\frac{u^2}{2} \frac{\partial}{\partial r} f(r), \quad (4.7a)$$

$$V_{22}(r) := -\frac{\partial}{\partial r} \frac{1}{2} Q_{22}(r) = -\frac{u^2}{2} \frac{\partial}{\partial r} g(r), \quad (4.7b)$$

$$V_{33}(r) = V_{22}(r), \quad (4.7c)$$

where

$$u^2 = \langle u_1^2 \rangle = \langle u_2^2 \rangle = \langle u_3^2 \rangle = \frac{1}{3} \langle \mathbf{u}^2 \rangle, \quad (4.8)$$

and $f(r) := Q_{11}(r)/u^2$ and $g(r) := Q_{22}(r)/u^2$ are the longitudinal and transverse velocity correlation functions, respectively.

Notably, our proposal for $V_{11}(r)$ (4.7a) can be related with a previous result. The kinematic relationship

$$\langle [\Delta v(r)]^2 \rangle = 2u^2[1 - f(r)], \quad (4.9)$$

can be rewritten as

$$\frac{1}{4} \frac{\partial}{\partial r} \langle [\Delta v(r)]^2 \rangle = -\frac{u^2}{2} \frac{\partial f}{\partial r}, \quad (4.10)$$

which, when substituted into (4.7a), leads to

$$3V_{11}(r) = \frac{\partial}{\partial r} \left[\frac{3}{4} \langle [\Delta v(r)]^2 \rangle \right]. \quad (4.11)$$

Note that this is the Townsend–Davidson function, $V_{TD}(r)$ (1.6). Now, because $V_{11}(r) \neq V_{22}(r)$, it follows that $V_{TD}(r) = 3V_{11}(r) \neq V(r)$ (where we have used (B1c)). We can now see why, starting from Townsend’s proposal, Davidson (2004) and Hamba (2015) arrived at disparate forms of energy-density functions.

5. Characteristic properties of spatial energy-density functions

In § 1, we listed three characteristic properties for a spatial energy-density function. Here, we consider each property in turn. For simplicity, we focus on homogeneous isotropic turbulence.

Interestingly, property (i) that a density function should be non-negative turns out to be the most difficult to satisfy. Indeed, to our knowledge, none of the functional forms proposed to date are guaranteed to be non-negative. The same is true for $V(r)$, $V_{11}(r)$ and $V_{22}(r)$. The reason can be understood by expressing these functions in terms of $E(k)$. Starting with the relationship

$$-\frac{1}{2} u^2 f(r) = \int_0^\infty dk E(k) G_1(kr), \quad G_1(x) = \frac{x \cos x - \sin x}{x^3}, \quad (5.1)$$

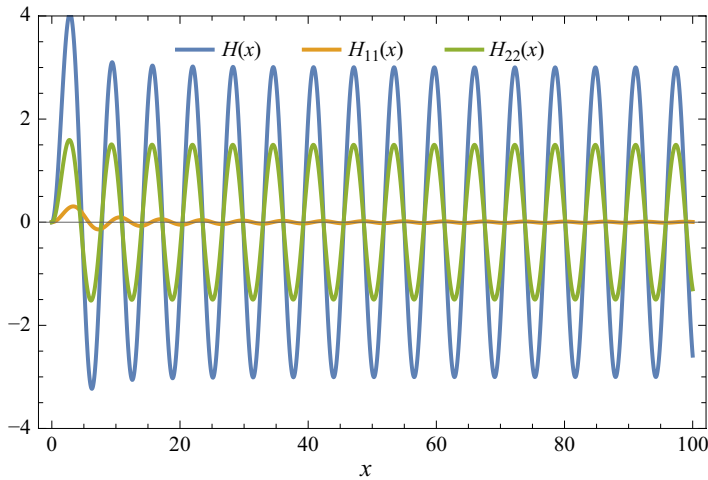


Figure 1. Shapes of the kernels $H(x)$, $H_{11}(x)$ and $H_{22}(x)$.

and using (4.11), (B1a), and (B1b), we can write

$$rV(r) = \int_0^\infty dk E(k) H(kr), \quad (5.2a)$$

$$rV_{11}(r) = \int_0^\infty dk E(k) H_{11}(kr), \quad (5.2b)$$

$$rV_{22}(r) = \int_0^\infty dk E(k) H_{22}(kr), \quad (5.2c)$$

where

$$\begin{aligned} H(kr) &= \frac{1}{r^3} \frac{\partial}{\partial r} [r^4 H_{11}(kr)], \\ H_{11}(kr) &= r \frac{\partial}{\partial r} G_1(kr), \\ H_{22}(kr) &= \frac{1}{2r^2} \frac{\partial}{\partial r} [r^3 H_{11}(kr)]. \end{aligned} \quad (5.3)$$

Now, since the kernels $H(x)$, $H_{11}(x)$ and $H_{22}(x)$ all oscillate about the x -axis taking positive and negative values (figure 1), $V(r)$, $V_{11}(r)$ and $V_{22}(r)$ are not guaranteed to be non-negative. Thus, strictly speaking, these functions are not density functions; Davidson (2004) suggested using the term ‘signature function’ instead. For simplicity, we shall refer to them as density functions.

Property (ii) expresses an energy constraint. Because we have derived $V(r)$ and its one-dimensional variants by imposing this constraint (cf. § 2), these functions satisfy the constraint by construction.

For checking property (iii), consider a random distribution of Townsend’s model eddies of a fixed size ℓ_e in a two-dimensional plane (Townsend 1976). For this turbulent flow, we can write $f(r) = \exp(-r^2/\ell_e^2)$. From (2.4) and (4.7), it follows that

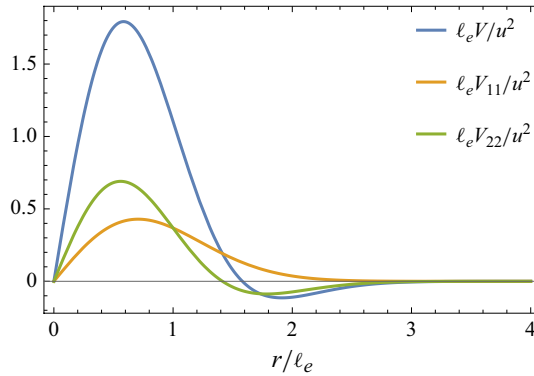


Figure 2. Distribution of energy across eddy sizes as quantified by $\ell_e V(r)/u^2$, $\ell_e V_{11}(r)/u^2$ and $\ell_e V_{22}(r)/u^2$ for a random distribution of Townsend's model eddies of fixed size ℓ_e .

$$\frac{\ell_e V(r)}{u^2} = (r/\ell_e) \left[5 - 2[(r/\ell_e)]^2 \right] \exp \left(-r^2/\ell_e^2 \right), \quad (5.4a)$$

$$\frac{\ell_e V_{11}(r)}{u^2} = (r/\ell_e) \exp \left(-r^2/\ell_e^2 \right), \quad (5.4b)$$

$$\frac{\ell_e V_{22}(r)}{u^2} = (r/\ell_e) \left[2 - [(r/\ell_e)]^2 \right] \exp \left(-r^2/\ell_e^2 \right). \quad (5.4c)$$

In [figure 2](#), we plot the energy distribution across eddy sizes from (5.4). In all cases, there is a clear peak around $r \sim \ell_e$. Notably, in this idealised flow, only $V_{11}(r)$ is non-negative for all r .

The above discussion of property (iii) points to a crucial advantage of one-dimensional spatial energy-density functions over their spectral counterparts. In the spectral space, this property reads: for a random distribution of eddies of fixed size ℓ_e , the corresponding $E(k)$ (or any of its one-dimensional variants) manifests a clear peak around $k \sim \ell_e^{-1}$ (Davidson 2004). While $E(k)$ satisfies this property, $E_{11}(k)$ and $E_{22}(k)$ do not. Instead of having a peak around $k \sim \ell_e^{-1}$, they attain their maxima at $k = 0$. (This is due to the phenomenon of aliasing (Davidson 2004).) As a result, it is difficult to interpret $E_{11}(k)$ and $E_{22}(k)$ in terms of eddy sizes, even though they satisfy the energy constraint. By contrast, as we have seen, $V_{11}(r)$ and $V_{22}(r)$ manifest a clear peak around $r \sim \ell_e$ ([figure 2](#)), underscoring their clear advantage over $E_{11}(k)$ and $E_{22}(k)$.

6. Analysis of empirical data

In § 4, we noted that one-dimensional spatial energy-density functions can be useful for analysis of empirical data. Here, for illustration, we analyse data from two canonical wall-bounded flows: channel flow and pipe flow. We take \hat{e}_1 along the streamwise direction, \hat{e}_2 along the wall-normal direction and \hat{e}_3 along the spanwise direction (for channel flow) or the azimuthal direction (for pipe flow). The origin of the coordinate system is at the wall (for channel flow) and the centreline (for pipe flow). Similar to most studies of empirical data, we focus on the case where the position x_2 is fixed and \mathbf{r} is oriented along \hat{e}_1 . Note that the flow is homogeneous along \hat{e}_1 (and \hat{e}_3), but not along \hat{e}_2 .

First, we consider the scaling $E_{11}(k_1) \propto k_1^{-1}$ (Perry, Henbest & Chong 1986). In the past decades, this scaling has attracted considerable attention and no small measure of debate (see, e.g. Smits, McKeon & Marusic (2011), Appendix A in Zamalloa *et al.* (2014)).

The scaling appears over a limited spatial region and at high Reynolds numbers, Re ; curiously, however, it disappears at even higher Re (Rosenberg *et al.* 2013; Yamamoto & Tsuji 2018). The range of k_1 for this scaling corresponds to the large eddies. In this regime, using Taylor's frozen-turbulence hypothesis may incur substantial errors. This limits the use of experimental data since most experiments obtain $E_{11}(k_1)$ using Taylor's hypothesis.

We analyse data from a direct numerical simulation (DNS) of channel flow at friction Reynolds number $Re_\tau \approx 5200$ (Lee & Moser 2015) ($Re_\tau := u_\tau \delta / \nu$, where u_τ is the friction velocity, δ the channel half-width and ν the kinematic viscosity). Lee & Moser (2015) noted that, over a small span of wall-normal distances ($90 \leq x_2^+ \leq 169$, where $x_2^+ := x_2 u_\tau / \nu$), the premultiplied spectrum $k_1 E_{11}(k_1)$ manifests a plateau, signalling $E_{11}(k_1) \propto k_1^{-1}$ (figure 3a). (Note that Taylor's hypothesis was not invoked to compute $E_{11}(k_1)$.) Expressed in the form of $V_{11}(r_1)$, $E_{11}(k_1) \propto k_1^{-1}$ scaling transforms to $V_{11}(r_1) \propto r_1^{-1}$. (This transformation follows from dimensional considerations: dimensionally, $[k_1 E_{11}(k_1)] = [r_1 V_{11}(r_1)]$, and thus, $E_{11}(k_1) \propto k_1^{-1}$ implies $V_{11}(r_1) \propto r_1^{-1}$.) In figure 3(b), we plot profiles of $r_1 V_{11}(r_1)$ corresponding to the spectra of figure 3(a). (We compute $V_{11}(r_1)$ from $E_{11}(k_1)$ using (C3a).) Unlike $k_1 E_{11}(k_1)$, $r_1 V_{11}(r_1)$ does not manifest a plateau for most of the spatial region except near $x_2^+ = 169$. By probing farther from the wall, we find a curious result. For $169 \leq x_2^+ \leq 191$, $k_1 E_{11}(k_1)$ does not manifest a plateau but $r_1 V_{11}(r_1)$ does so (figure 4). Thus, $V_{11}(r_1) \propto r_1^{-1}$ scaling prevails over a region that is spatially contiguous to albeit shifted from the $E_{11}(k_1) \propto k_1^{-1}$ scaling region. The results suggest that the spatial domain of the scaling region depends on the diagnostic function employed to evince the scaling.

In figure 3(a), we note the bimodal structure of $k_1 E_{11}(k_1)$, wherein the k_1^{-1} scaling regime is flanked on its sides by two local peaks. These peaks are considered to be signatures of organised motions at large scales, the left peak corresponding to 'very-large-scale motions' (VLSMs) and the right peak to 'large-scale motions' (LSMs) (Kim & Adrian 1999). We represent these peaks as k_1^{VLSM} and k_1^{LSM} , respectively. The attendant eddy sizes are estimated as $\ell_{VLSM} = 2\pi / k_1^{VLSM}$ and $\ell_{LSM} = 2\pi / k_1^{LSM}$, respectively. From figure 3(a), we find $\ell_{VLSM} \approx 6\delta$ and $\ell_{LSM} \approx 0.3\delta$. That organised motions exist at scales $\gtrsim \delta$, as is the case with VLSMs, is a surprising finding and an active area of inquiry (Smits *et al.* 2011).

We wish to draw attention to some potential problems in inferring the eddy sizes using $2\pi / k_1$. As discussed in § 1, eddies are not waves – consequently, the wavelength of a Fourier mode may not directly correspond to an eddy size. More important, as we have noted in § 5, it is difficult to infer eddy sizes from $E_{11}(k_1)$. Shifting from the Fourier space to the real space may prove useful. Interestingly, similar to its spectral counterpart, $r_1 V_{11}(r_1)$ also manifests a bimodal structure (figure 3b). Analogous to the discussion of the peaks of $k_1 E_{11}(k_1)$, we can ascribe the left peak to signal LSMs and the right peak to signal VLSMs. The attendant eddy sizes can be estimated as the values of r_1 corresponding to these peaks. We find $\ell_{LSM} \approx 0.03\delta$ and $\ell_{VLSM} \approx 0.8\delta$. Notably, now the organised motions inhabit scales $\lesssim \delta$, consistent with the standard conceptual picture of turbulent eddies. We suggest that an extensive study of empirical data on wall-bounded flows along these lines may yield valuable insights into the structure of organised motions at large scales.

Returning to the k_1^{-1} and r_1^{-1} scalings, we now turn attention to components other than $E_{11}(k_1)$ and $V_{11}(r_1)$. Specifically, we consider $E_{33}(k_1)$ and $V_{33}(r_1)$ for DNS of channel flow at $Re_\tau = 2000$ (Lee & Moser 2015). (We compute $V_{33}(r_1)$ from $E_{33}(k_1)$ using (C3c).) Over the span $902 \leq x_2^+ \leq 1198$, it is difficult to discern a plateau in $k_1 E_{33}(k_1)$ (figure 5a).

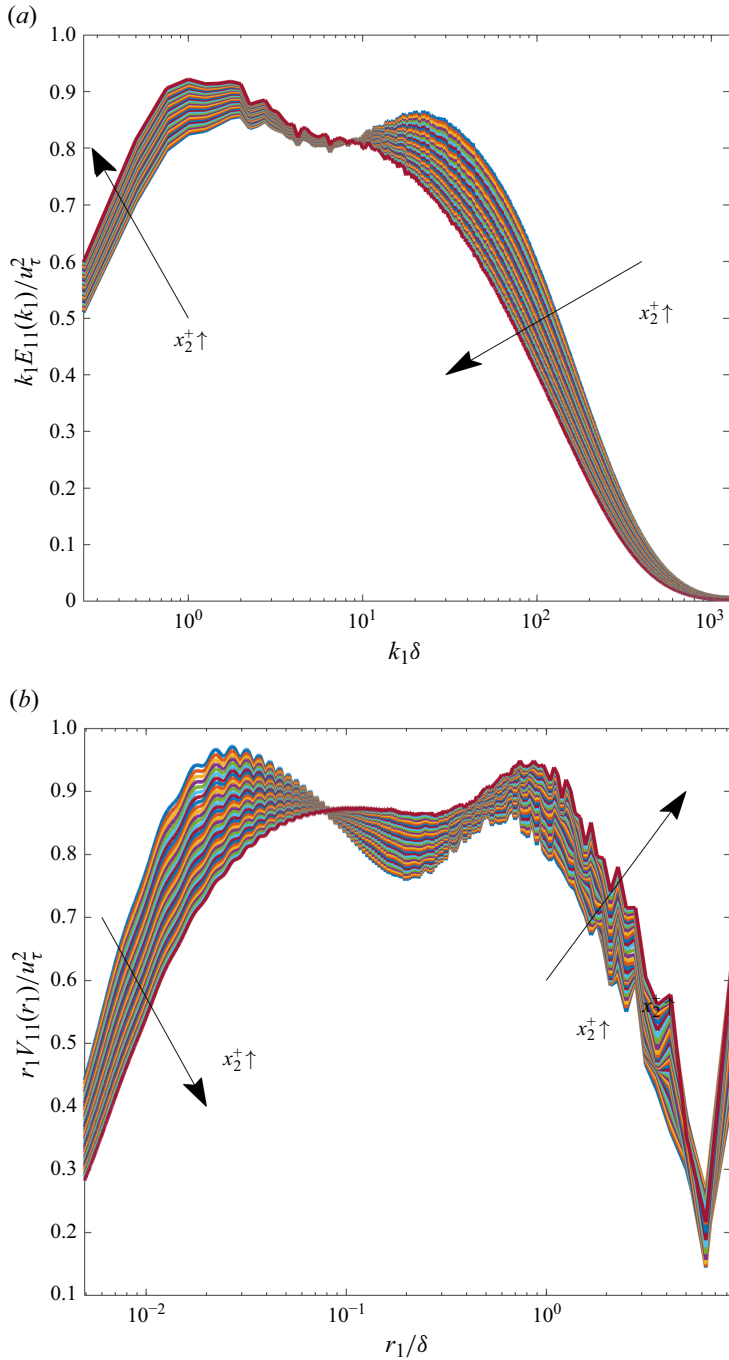


Figure 3. Testing the k_1^{-1} and r_1^{-1} scalings for DNS of channel flow at $Re_\tau \approx 5200$ (Lee & Moser 2015): (a) normalised premultiplied spectrum $k_1 E_{11}(k_1)/u_\tau^2$ and (b) normalised premultiplied spatial energy-density function $r_1 V_{11}(r_1)/u_\tau^2$. Each curve corresponds to a fixed value of x_2^+ in the range $x_2^+ \in [90, 169]$.

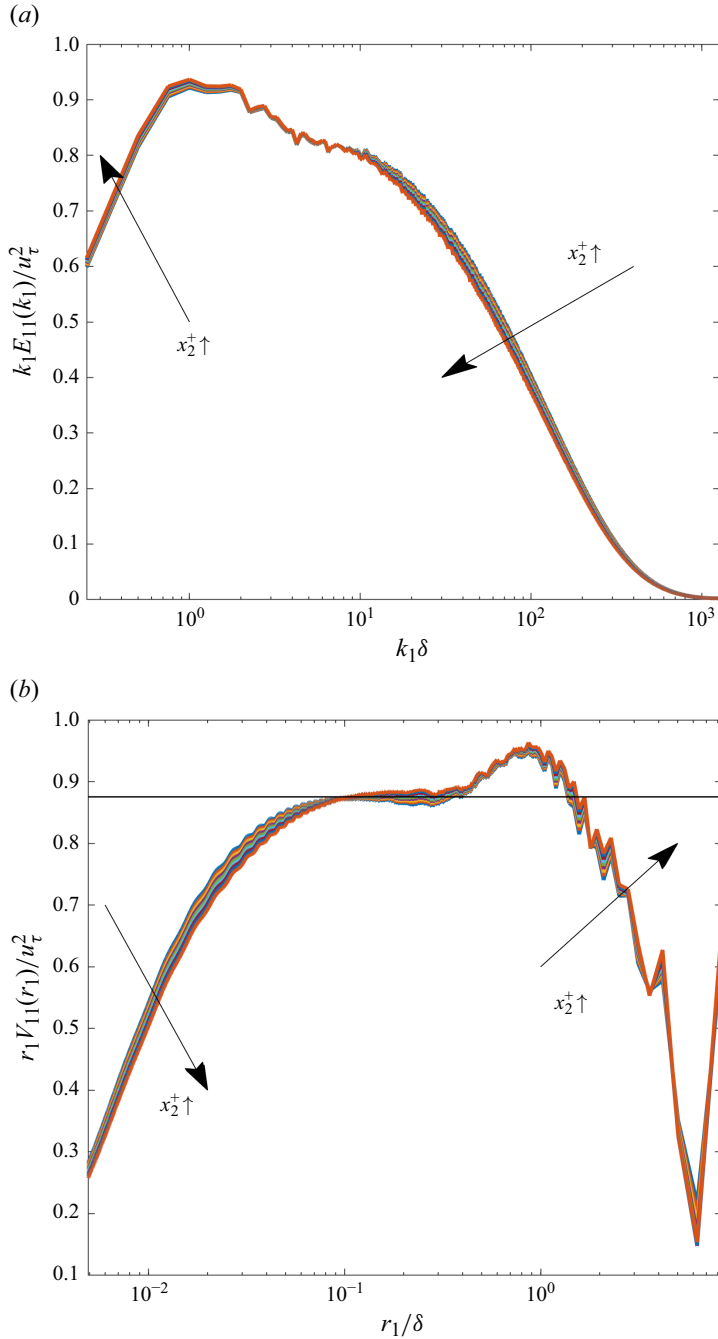


Figure 4. Testing the k_1^{-1} and r_1^{-1} scalings for DNS of channel flow at $Re_\tau \approx 5200$ (Lee & Moser 2015): (a) normalised premultiplied spectrum $k_1 E_{11}(k_1)/u_\tau^2$ and (b) normalised premultiplied spatial energy-density function $r_1 V_{11}(r_1)/u_\tau^2$. Each curve corresponds to a fixed value of x_2^+ in the range $x_2^+ \in [169, 191]$. In the nominal r_1^{-1} scaling regime, $0.1 \lesssim r_1/\delta \lesssim 0.3$, the plateau value $r_1 V_{11}(r_1)/u_\tau^2 \approx 0.88$ (black line, panel b).

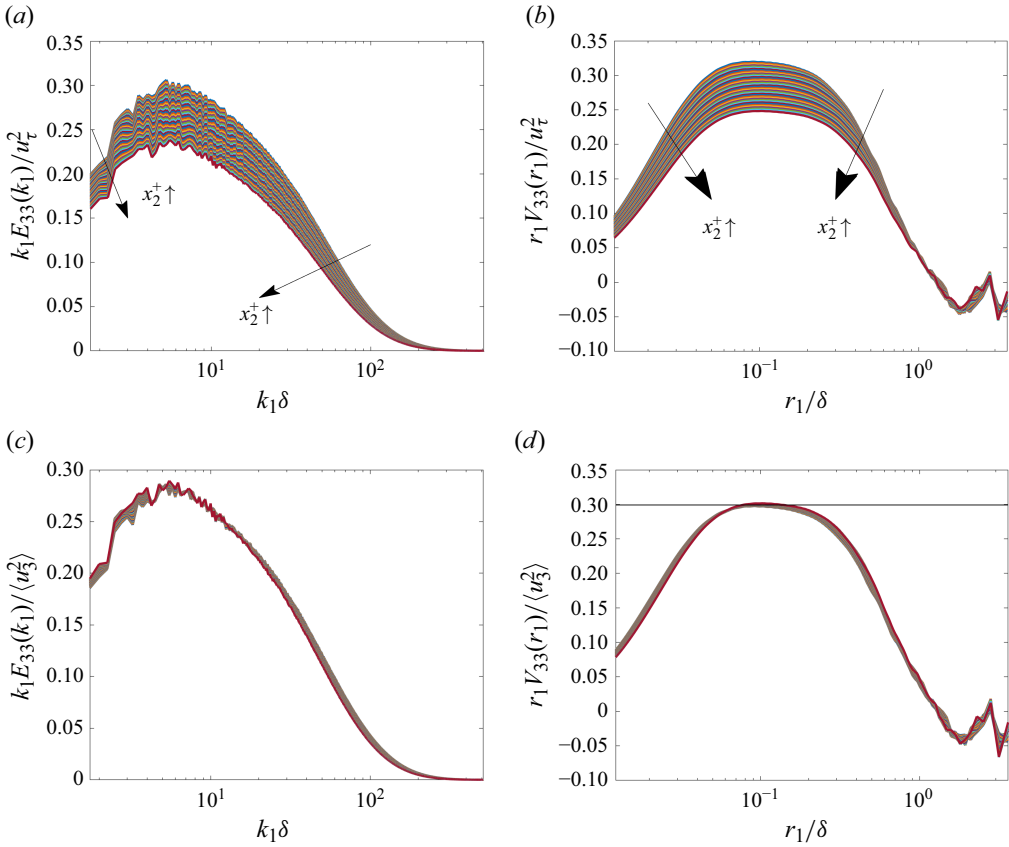


Figure 5. Testing the k_1^{-1} and r_1^{-1} scalings for DNS of channel flow at $Re_\tau = 2000$ (Lee & Moser 2015): (a) normalised premultiplied spectrum $k_1 E_{33}(k_1)/u_\tau^2$; (b) normalised premultiplied spatial energy-density function $r_1 V_{33}(r_1)/u_\tau^2$; (c) normalised premultiplied spectrum $k_1 E_{33}(k_1)/\langle u_3^2 \rangle$; (d) normalised premultiplied spatial energy-density function $r_1 V_{33}(r_1)/\langle u_3^2 \rangle$. Each curve corresponds to a fixed value of x_2^+ in the range $x_2^+ \in [902, 1198]$. In the nominal r_1^{-1} scaling regime, $0.07 \lesssim r_1/\delta \lesssim 0.17$, the plateau value $r_1 V_{33}(r_1)/\langle u_3^2 \rangle \approx 0.3$ (black line, panel d).

By contrast, $r_1 V_{33}(r_1)$ manifests a plateau, signalling $V_{33}(r_1) \propto r_1^{-1}$ (figure 5b). Unlike the case in figure 3(b), the plateau for the curves corresponding to different x_2^+ positions do not collapse when normalised as $r_1 V_{33}(r_1)/u_\tau^2$. But, when normalised as $r_1 V_{33}(r_1)/\langle u_3^2 \rangle$, they collapse (figure 5d). (The normalised curves for $k_1 E_{33}(k_1)/\langle u_3^2 \rangle$ also collapse, but unlike its real-space counterpart, there is no plateau; figure 5(c).) Remarkably, the collapse occurs not only in the plateau region, but over the whole range of r_1 . In figure 5(b), we can also see one drawback of $V_{33}(r_1)$ – it becomes negative for $r_1 > \delta$. It does, however, satisfy a weaker condition, $\int_0^{r_1} dr_1 V_{33}(r_1) \geq 0$ (Davidson 2004).

A few additional remarks on the $V_{33}(r_1) \propto r_1^{-1}$ scaling may be useful. Because the definition of $V_{33}(r_1)$ is a new result, this scaling and the attendant collapse of $r_1 V_{33}(r_1)/\langle u_3^2 \rangle$ are novel findings. It is worth noting that, to our knowledge, the spectral counterpart of this scaling, $E_{33}(k_1) \propto k_1^{-1}$, has not been reported, which adds to the novelty of the $V_{33}(r_1) \propto r_1^{-1}$ scaling. Further, we observed this scaling for channel flow

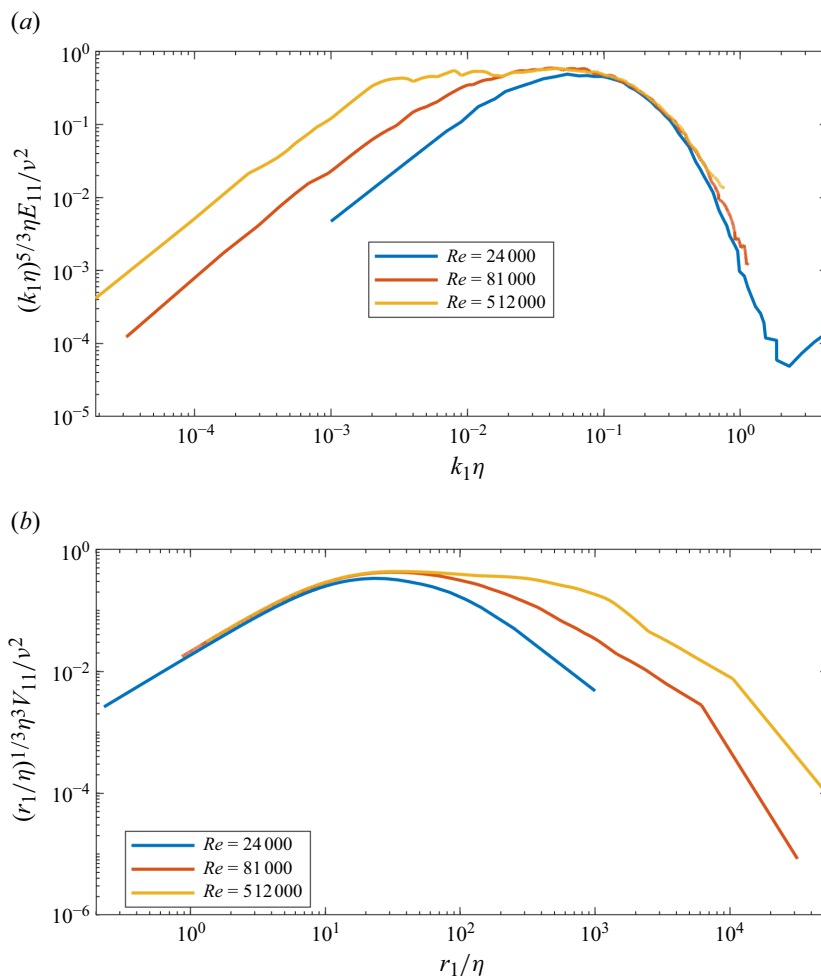


Figure 6. Testing the $k_1^{-5/3}$ and $r_1^{-1/3}$ scalings at the centreline of a pipe flow from the Princeton superpipe experiment (Bailey *et al.* 2009; Rosenberg *et al.* 2013): (a) normalised premultiplied spectrum $(k_1 \eta)^{5/3} \eta E_{11}(k_1) / v^2$; (b) normalised premultiplied spatial energy-density function $(r_1 / \eta)^{1/3} \eta^3 V_{11}(r_1) / v^2$. The data correspond to $Re := UD/\nu = 24\,000$, $81\,000$, $512\,000$, where U is the mean flow velocity and D is the pipe diameter.

at $Re_\tau = 2000$ but not at $Re_\tau = 1000$ or $Re_\tau \approx 5200$. It would appear that, similar to the $E_{11}(k_1) \propto k_1^{-1}$ scaling, this scaling is also limited to a finite range of Re_τ .

Unlike the k_1^{-1} scaling, the classical Kolmogorov inertial-range scaling, $k^{-5/3}$, and the related phenomenon of small-scale universality manifest systematic trends with increase of Re (Kolmogorov 1941). To illustrate these trends, we turn to experimental measurements of $E_{11}(k_1)$ at the centreline of a pipe from the high- Re Princeton superpipe experiment (Bailey *et al.* 2009; Rosenberg *et al.* 2013). In figure 6(a), we plot the premultiplied spectrum $k_1^{5/3} E_{11}(k_1)$. For $Re \gtrsim 81\,000$, a plateau emerges, signalling $E_{11}(k_1) \propto k_1^{-5/3}$. With increase in Re , the plateau broadens. Moreover, the spectra normalised in Kolmogorov units collapse onto a universal curve at the small scales (at large $k_1 \eta$, where η is the Kolmogorov length scale), signalling small-scale universality.

The collapsed region broadens with increase in Re . (This collapse persists even for low- Re transitional pipe flow (Cerbus *et al.* 2020).) The spatial counterpart of the $E_{11}(k_1) \propto k_1^{-5/3}$ scaling is $V_{11}(r_1) \propto r_1^{-1/3}$. (This follows from dimensional considerations: using $[k_1 E_{11}(k_1)] = [r_1 V_{11}(r_1)]$, $E_{11}(k_1) \propto k_1^{-5/3}$ and $k_1 \propto r_1^{-1}$, we obtain $V_{11}(r_1) \propto r_1^{-1/3}$.) In figure 6(b), we plot the profiles of $r_1^{1/3} V_{11}(r_1)$ corresponding to the spectra of figure 6(a). Complementary to the spectral results, we note a plateau emerging and broadening with increase in Re . Similarly, we note a collapse onto a universal curve at small scales, with the collapsed region broadening with increase in Re .

7. Concluding remarks

Quantifying turbulent kinetic energy distribution in the real space via a spatial energy-density function has been a long-standing quest. Basing our analysis on an energy constraint, in §2, we derived $V(r)$ for homogeneous isotropic turbulence. In §3, we generalised this derivation to anisotropic flows. Our analysis till that point focused on a three-dimensional spatial energy-density function. In §4, we introduced the concept of one-dimensional spatial energy-density functions.

Although one-dimensional energy-density functions are well known in the spectral space, that is not the case for the real space. Correspondingly, distinctions between the three-dimensional $V(r)$ and its one-dimensional variants have not been recognised previously. Indeed, this allowed us to resolve the discrepancies between the Townsend–Davidson function $V_{TD}(r)$ and the Townsend–Hamba function $V_{TH}(r)$. While both share the same starting point – Townsend’s pioneering proposal of (1.5) – we showed that $V_{TD}(r)$ corresponds to $3V_{11}(r)$ whereas $V_{TH}(r)$ corresponds to $V(r)$.

A distinctive feature of one-dimensional spatial energy-density functions is that they satisfy the crucial requirement that allows for a one-to-one correspondence with eddy sizes (cf. property (iii) discussed in §1). Their spectral counterparts, on the other hand, do not satisfy this requirement and thus do not allow for a one-to-one correspondence with eddy sizes. This property makes one-dimensional spatial energy-density functions particularly attractive for the analysis of empirical data. In §6, we discuss illustrative examples of such analysis. Some of the notable findings from this analysis include: a new spatial region of $V_{11}(r_1) \propto r_1^{-1}$ scaling (figure 4); a new scaling regime of $V_{33}(r_1) \propto r_1^{-1}$ (figure 5d); and a potential solution to the puzzlingly large sizes of VLSMs.

In closing, we wish to draw attention to a critical unfinished task. The fact that in Townsend’s formalism $V(r)$, $V_{11}(r)$ and $V_{22}(r)$ are all not guaranteed to be non-negative is a drawback that is shared by other functions proposed in the literature (Davidson & Pearson 2005; Hamba 2015). To our knowledge, no function satisfying the non-negative property has been rigorously developed. As such, there is no proposal that strictly satisfies all three properties necessary for a spatial energy-density function. We submit that finding such a function may yield promising dividends.

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Appendix A. Deriving $V(r)$ for homogeneous isotropic turbulence using Townsend’s approach

Here, we derive (2.4) for $V(r)$ starting with Townsend’s main result, (1.5). First, we note that (1.5) needs two modifications: (i) the minus sign should not be there as it would lead

to negative energy; (ii) we introduce an additional factor of $1/2$ since the resulting function should represent the turbulent kinetic energy-density function and integrate to $(1/2)\langle u^2 \rangle$. Now, because (1.5) is expressed in per unit range of $d(\log r)$, we multiply (1.5) (with the above-mentioned modifications) by $d(\log r)$ to obtain the contributions to $(1/2)\langle u_1^2 \rangle$ from eddies of size in the range $(r, r + dr)$

$$r \frac{\partial}{\partial r} \frac{1}{4} [S_{11}(r)] d(\log r) = \frac{\partial}{\partial r} \frac{1}{4} [S_{11}(r)] dr. \quad (\text{A1})$$

To derive a three-dimensional spatial energy-density function, (A1) can be easily extended to include the contributions to $\langle (1/2)u_2^2 \rangle$ and $\langle (1/2)u_3^2 \rangle$. Summing them up, contributions to $(1/2)\langle u^2 \rangle$ from eddies of size in the range $(r, r + dr)$ can be expressed as

$$V(r)dr = \frac{1}{4} \frac{\partial}{\partial r} S_{ii}(r) dr, \quad (\text{A2})$$

with summation over repeating indices implied. Using the relation

$$S_{ii}(r) = 2Q_{ii}(0) - 2Q_{ii}(r), \quad (\text{A3})$$

equation (A2) can be written as

$$V(r) = -\frac{\partial}{\partial r} \frac{1}{2} Q_{ii}(r), \quad (\text{A4})$$

which is (2.4).

We note that the starting point of the derivation discussed above is Townsend's proposal, (1.5). We have attempted to demonstrate in a clear manner how it leads to $V(r)$. But, if we consider (1.5) itself, Townsend's reasoning is not entirely clear. Thus, in this manuscript, we derive (2.4) using a different approach (cf. § 2).

Appendix B. Some kinematic relationships between spatial energy-density functions (isotropic turbulence)

In the spectral space, kinematic relationships between $E(k)$ and its one-dimensional variants are well known. In the same vein, the following kinematic relationships between $V(r)$ and its one-dimensional variants can be readily established

$$V(r) = \frac{1}{r^3} \frac{\partial}{\partial r} [r^4 V_{11}(r)], \quad (\text{B1a})$$

$$V_{22}(r) = \frac{1}{2r^2} \frac{\partial}{\partial r} [r^3 V_{11}(r)], \quad (\text{B1b})$$

$$V(r) = V_{11}(r) + 2V_{22}(r), \quad (\text{B1c})$$

$$\frac{\partial}{\partial r} [r^3 V(r)] = \frac{2}{r} \frac{\partial}{\partial r} [r^4 V_{22}(r)]. \quad (\text{B1d})$$

Appendix C. Relationships between one-dimensional spatial and spectral energy-density functions

For analysis of empirical data, it is useful to obtain relationships between the spectral and spatial variants of the one-dimensional energy-density functions. In the direction $\mathbf{r} = r_1 \hat{\mathbf{e}}_1$, the spectral one-dimensional energy-density functions are defined as

$$E_{11}(k_1) = \frac{1}{\pi} \int_0^\infty dr_1 Q_{11}(r_1 \hat{\mathbf{e}}_1) \cos(k_1 r_1), \quad (\text{C1a})$$

$$E_{22}(k_1) = \frac{1}{\pi} \int_0^\infty dr_1 Q_{22}(r_1 \hat{\mathbf{e}}_1) \cos(k_1 r_1), \quad (\text{C1b})$$

$$E_{33}(k_1) = \frac{1}{\pi} \int_0^\infty dr_1 Q_{33}(r_1 \hat{\mathbf{e}}_1) \cos(k_1 r_1), \quad (\text{C1c})$$

and the inverse cosine transform transforms are

$$Q_{11}(r_1 \hat{\mathbf{e}}_1) = 2 \int_0^\infty dk_1 E_{11}(k_1) \cos(k_1 r_1), \quad (\text{C2a})$$

$$Q_{22}(r_1 \hat{\mathbf{e}}_1) = 2 \int_0^\infty dk_1 E_{22}(k_1) \cos(k_1 r_1), \quad (\text{C2b})$$

$$Q_{33}(r_1 \hat{\mathbf{e}}_1) = 2 \int_0^\infty dk_1 E_{33}(k_1) \cos(k_1 r_1). \quad (\text{C2c})$$

From the inverse transform pairs, it can be readily confirmed that

$$V_{11}(r_1) = \int_0^\infty dk_1 k_1 E_{11}(k_1) \sin(k_1 r_1), \quad (\text{C3a})$$

$$V_{22}(r_1) = \int_0^\infty dk_1 k_1 E_{22}(k_1) \sin(k_1 r_1), \quad (\text{C3b})$$

$$V_{33}(r_1) = \int_0^\infty dk_1 k_1 E_{33}(k_1) \sin(k_1 r_1), \quad (\text{C3c})$$

and the associated forward transforms are

$$k_1 E_{11}(k_1) = \frac{2}{\pi} \int_0^\infty dr_1 V_{11}(r_1) \sin(k_1 r_1), \quad (\text{C4a})$$

$$k_1 E_{22}(k_1) = \frac{2}{\pi} \int_0^\infty dr_1 V_{22}(r_1) \sin(k_1 r_1), \quad (\text{C4b})$$

$$k_1 E_{33}(k_1) = \frac{2}{\pi} \int_0^\infty dr_1 V_{33}(r_1) \sin(k_1 r_1). \quad (\text{C4c})$$

Appendix D. Transport equation for $V(r, t)$

In the manuscript, we focused on kinematics of spatial energy-density functions. To study the dynamics, we can analyse their transport equations (Davidson & Pearson 2005; Hamba 2015). As an illustration, here, focusing on homogeneous isotropic turbulence, we follow the approach of Davidson & Pearson (2005) to derive and analyse the transport equation for $V(r, t)$, where t is the time. (In the manuscript, we did not explicitly note the dependence on time as our focus was on kinematics.)

Our starting point is the transport equation for $(1/2)Q_{ii}(r, t)$, which is the Kármán–Howarth equation (Davidson 2004)

$$\frac{\partial}{\partial t} \frac{1}{2} Q_{ii}(r, t) = \frac{\partial}{\partial r} \Gamma(r, t) + \frac{\nu}{r^2} \frac{\partial}{\partial r} r^2 \frac{\partial Q_{ii}}{\partial r}, \quad (\text{D1})$$

where

$$\Gamma(r, t) = \int_0^r ds \frac{1}{12s^2} \frac{\partial}{\partial s} \frac{1}{s} \frac{\partial}{\partial s} [s^4 S_3(s, t)], \quad (\text{D2})$$

and the third-order structure function is defined as $S_3(r, t) := \langle [\Delta v(r, t)]^3 \rangle$. Combining (D1) with (2.4)

$$V(r, t) = -\frac{\partial}{\partial r} \frac{1}{2} Q_{ii}(r, t), \quad (\text{D3})$$

yields the transport equation for $V(r, t)$

$$\frac{\partial}{\partial t} V(r, t) = \frac{\partial}{\partial r} \Pi_V(r, t) + 2\nu \frac{\partial}{\partial r} \frac{1}{r^2} \frac{\partial}{\partial r} [r^2 V(r, t)], \quad (\text{D4})$$

where we have defined the spatial energy flux $\Pi_V(r, t)$ as

$$\Pi_V(r, t) := -\frac{1}{12r^2} \frac{\partial}{\partial r} \frac{1}{r} \frac{\partial}{\partial r} [r^4 S_3(r, t)]. \quad (\text{D5})$$

The spectral counterpart to (D4) is (Davidson 2004)

$$\frac{\partial}{\partial t} E(k, t) = -\frac{\partial}{\partial k} \Pi_E(k, t) - 2\nu k^2 E(k, t), \quad (\text{D6})$$

where $\Pi_E(k, t)$ is the spectral kinetic energy flux. In analogy with the spectral energy transfer $T_E(k, t) = -\partial \Pi_E / \partial k$, we can define the spatial energy transfer density function

$$T_V(r, t) := \frac{\partial \Pi_V}{\partial r}. \quad (\text{D7})$$

It has the conservative property that $\int_0^\infty dr T_V = 0$.

It is instructive to consider the transfer of energy from eddies of size $\geq r$ to eddies of size $\leq r$. To do this, we integrate (D4) over $r \rightarrow s \in [r, \infty]$ for some arbitrary r

$$\begin{aligned} \frac{\partial}{\partial t} \int_r^\infty ds V(s, t) &= \int_r^\infty ds \frac{\partial}{\partial s} \Pi_V(s, t) + 2\nu \int_r^\infty ds \frac{\partial}{\partial s} \frac{1}{s^2} \frac{\partial}{\partial s} [s^2 V(s, t)] \\ &= -\int_0^r ds \frac{\partial}{\partial s} \Pi_V(s, t) - \int_r^\infty ds D(s, t), \end{aligned} \quad (\text{D8})$$

where we have defined the dissipation density as

$$D(r, t) := -2\nu \frac{\partial}{\partial r} \frac{1}{r^2} \frac{\partial}{\partial r} [r^2 V(r, t)]. \quad (\text{D9})$$

Equation (D8) can be interpreted as follows: the loss of energy from eddies of size $\geq r$ is due to the transfer to eddies of size $\leq r$ (via $\Pi_V(r, t)$) and direct loss to viscous dissipation (via $D(r, t)$). In other words, equation (D4) embodies an energy cascade in the real space.

We can also analyse the inertial range. Integrating (D4) yields

$$\int_0^r ds \frac{\partial}{\partial t} V(s, t) = \Pi_V(r, t) + \frac{2\nu}{r^2} \frac{\partial}{\partial r} [r^2 V] - \lim_{r \rightarrow 0} \frac{2\nu}{r^2} \frac{\partial}{\partial r} [r^2 V]. \quad (\text{D10})$$

Next, recall that when the turbulence is locally isotropic, the velocity derivative moments are related by

$$\left\langle \frac{\partial u_i}{\partial x_j} \frac{\partial u_i}{\partial x_j} \right\rangle = -\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial Q_{ii}}{\partial r} \right) \Big|_{r=0} = \langle \omega^2 \rangle, \quad (\text{D11})$$

where $\langle \omega^2 \rangle$ is the mean enstrophy. This standard result can then be expressed in terms of the spatial energy density V as

$$\lim_{r \rightarrow 0} \frac{2\nu}{r^2} \frac{\partial}{\partial r} [r^2 V(r, t)] = \nu \langle \omega^2 \rangle = \varepsilon. \quad (\text{D12})$$

Finally, substituting (D12) into (D10) we arrive at the integrated form of the transport equation

$$\int_0^r ds \frac{\partial}{\partial t} V(s, t) = \Pi_V(r, t) + \frac{2\nu}{r^2} \frac{\partial}{\partial r} [r^2 V] - \varepsilon. \quad (\text{D13})$$

Now, focusing on the inertial-range eddies, we invoke the standard assumptions that the turbulence is locally stationary (so the time-derivative term on the left-hand side is zero) and that the viscous term is negligible. This yields the scale invariance of the spatial energy flux in the inertial range

$$\Pi_V(r, t) = \varepsilon. \quad (\text{D14})$$

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